Correction of cone index for soil water content differences in a coastal plain soil

W.J. Busscher [a,*], P.J. Bauer [a], C.R. Camp [a], R.E. Sojka [b]

[a] *Coastal Plains Soil, Water, and Plant Research Center, USDA-ARS, Florence, SC, USA*
[b] *Northwest Irrigation and Soils Research Lab, USDA-ARS, Kimberly, ID, USA*

Abstract

Soil penetration resistance (cone index) varies with water content. The field variation of water content could mask treatment differences. The correction of cone index data to a single water content would help prevent this. We used equations from TableCurve™ software and from the literature to correct cone indices for differences in soil water contents. Data were taken from two field experiments where cotton (*Gossypium hirsutum* L.) was grown using conventional and conservation tillage without irrigation, and beans (*Phaseolus vulgaris* L.) were grown using conventional tillage with microirrigation. Boundary conditions based on hard, dry and soft, wet soils were imposed on the equations. Equations fit the data with coefficients of determination ranging from 0.55 to 0.92 and error mean squares from 1.37 to 6.35. After correction, cone index dependence on water content was reduced. A single-equation correction did not always fit the data across all treatments. Separate corrections, based on treatment, might be required. When corrections required multiple equations, differences may be real or may be a manifestation of the correction differences. In this case, the correction may not be feasible (unless some future work can coordinate different equations and assure a uniform correction). © 1997 Elsevier Science B.V.

Keywords: Soil strength; Penetrometer; Soil water; Cone index; Coastal plain

1. Introduction

Soil penetration resistance as measured by cone index varies with other soil properties such as water content, bulk density, texture, and organic matter (Taylor and Gardner, 1963; Camp and Lund, 1968; Mirreh and Ketcheson, 1972; Spivey et al., 1986;

---

* Corresponding author.

Perumpral, 1987; Ley et al., 1993). Field soil water contents can vary considerably in time and space. This variation and its effect on penetration resistance might mask imposed treatment differences. Correcting penetration resistance for differences in soil water content could reduce or eliminate the water content effect on it and improve our measurement and understanding of the impact of management practices on penetration resistance.

Adjustments of flat-tipped, laboratory penetrometer data to a common water content have been successful (Busscher, 1990), while corrections for cone-tipped, field penetration resistance in the same study were not. Asady et al. (1987) accounted for water content as a continuous covariate of cone index in an analysis of variance (ANOVA). Others have accounted for cone index dependence on water content using this type of analysis (Yasin et al., 1993).

Several researchers have worked on the relationship between penetration resistance and soil water content. Among them are Ayers and Perumpral (1982). They found a direct relationship between cone index and bulk density and an inverse relationship between cone index and water content squared for various mixtures of sand and clay. Ohu et al. (1988), on the other hand, found an exponential relationship between cone index and water content for loams and clays. Their equation also included applied compaction pressure, shear strength, and overburden pressure. Ley et al. (1995) found a linear correlation between penetration resistance and water content and a nonsignificant, general relationship between penetration resistance and bulk density. Martino and Shaykewich (1994) found a relationship between penetration resistance and time as water content changed within different tillage systems. Ley and Laryea (1994) used spatial statistics to show a general relationship between penetration resistance and water content. Even with a lubricated penetrometer (Tollner and Verma, 1987), cone index and water content interactions were found to be complex.

All empirical and conceptual models that have been proposed to explain penetration resistance include water content as an independent variable. An empirical, mathematical relationship that represents the dependence of cone index on water content can help us understand the relationship between the two. The relationship can help clarify the effect of spatial differences by correcting data to a common water content. Such a relationship could also be useful for simulations, especially when soil strength and water content are considered as inputs for predicting root growth (Martino and Shaykewich, 1994; Unger and Kaspar, 1994).

Our objective was to find and use a generalized empirical relationship between cone index and water content that reduced or eliminated the dependence of cone indices on water content for massive-structured, sandy Coastal Plain soils.

2. Materials and methods

2.1. Sources of equations

Cone indices from field experiments were used to test equations that corrected data for differences in water content. We obtained equations developed for this and other

purposes in the literature and from TableCurve [1] curve fitting software that uses the least squares method (Jandel Scientific, Corte Madera, CA). TableCurve suggested several hundred equations. We limited the choices based on boundary conditions and on simplicity of the equation. Boundary conditions, based on field experience, were cone indices of zero at or near saturation and high strength (offscale, i.e., > 10 MPa) at low (< 0.01 g/g) water contents. The simplicity of equations was based on visual judgement of the fit of the equation to the data. Some equations fit the data more closely than those chosen. However, they had a tortuous fit, winding through data points, but not representing any data trend or physical reality. They were ignored.

The equations chosen were:

$$C = aW^b, \tag{1}$$

$$C = a(1 - W)^b, \tag{2}$$

$$C = ae^{bW}, \tag{3}$$

where C is cone index in MPa, W is water content on a dry weight basis in g/g, e is the base of natural logarithms, and a and b are empirical parameters that will be calculated and compared throughout the text. Eq. (1) to Eq. (3) can be found in the literature. Eqs. (1) and (2) were proposed by Mielke et al. (1994). They used the equations to solve for water content knowing cone index. We used them in a transposed form to find cone index from water content. Eq. (3) is similar to an equation used to correct flat-tipped penetrometer data (Busscher, 1990). We chose to adapt these equations for use on cone-tipped penetrometer data for sandy Coastal Plain soils.

2.2. Limitations

The boundary condition of high strength at low water content may be a result of cementation, similar to that seen by Bresson and Moran (1995). This may not be suitable for other soils.

As seen in Section 1, relationships involving cone index and water content, and a variety of other variables have been developed. We assumed that a relationship between cone index and water content could be developed, independent of other variables.

Other equations, similar to Eqs. (1)–(3), fit the data. For example, $C = aW^{-1}$ was a good fit. However, this was a specific case of Eq. (1) where $b = -1$.

2.3. Sources of data

The data used in the experiment were taken from two soil management experiments. The first was a cotton (var. Coker 315) experiment performed in 1991 and 1992 at the

---

[1] Mention of trademark, proprietary product, or vendor does not constitute a guarantee or warranty of the product by the US Dept. of Agric. and does not imply its approval to the exclusion of other products or vendors that may also be suitable.

Clemson Pee Dee Research and Education Center in Florence, SC, USA (Bauer and Busscher, 1996). The soil was a Norfolk loamy sand (fine, loamy, siliceous, thermic, Typic Kandiudult). The Norfolk soil has a massive structure and at times may exhibit very weak subangular blocky structure. Cotton was grown on beds that rose 5–10 cm above the mid-rows. Row widths were 0.96 m.

The experimental field design was randomized complete blocks in a split–split plot arrangement. Main plots were cover crops of vetch (*Vicia villosa*, Roth) and no cover. Subplots were conventional and conservation tillage, and sub-subplots were depths of measurement. Main plots were 8-m wide by 30-m long, divided evenly between tillage treatments.

Conventional tillage plots were spring disked and rebedded. Conservation tillage plots were not disked. In conservation tillage plots, beds were reformed by throwing 2.5 cm or less of soil onto the existing beds with a cultivator before seeding the cover crop in fall. Both conventional and conservation tillage included in-row subsoiling to a depth of 25–30 cm at the time of planting.

Soil strength readings were taken as cone indices on October 1, 1991, and October 26, 1992, shortly after cotton harvest. Cone indices were taken with a 13-mm diameter, 30° solid angle cone tip, hand-operated, recording penetrometer (Carter, 1967). The penetrometer recorded cone indices to 0.55-m depths. Three probings were taken in each plot along the nonwheel-track mid row and digitized into the computer using the method of Busscher et al. (1985). Soil water contents were taken at 10-cm-depth intervals and associated with the corresponding cone index readings at that depth.

Cone indices from the surface 25 cm were ignored because of spring disking in some treatments and spring or fall bedding. Readings were taken in the nonwheel tracks to develop a relationship between cone index and water content without interference from traffic or tillage. Another reason for starting to take readings at 25 cm is that the root-limiting E horizon in this soil, a hardpan, begins at this depth (Doty et al., 1975).

The equations were also used on data from a green bean (cv. Bush Blue Lake 274) experiment. Plots were established in 1984 at the Coastal Plains Soil, Water, and Plant Research Center near Florence, SC, USA, approximately 15 km from the site of the cotton experiment. We conducted the bean experiment on these plots during the summers of 1988 and 1989 (Camp et al., 1993). The soil within the plots was also a Norfolk loamy sand with a hardpan below the plow layer.

The field design was randomized complete blocks with four replications. Treatments were irrigated with microirrigation tubing. There were two treatments, placement of the microirrigation tube and frequency of irrigation, with two levels each. Tubes were placed at 0.75-m intervals either on the surface immediately next to each row or buried at approximately 0.25 m below the rows. Irrigation was applied at two frequencies: high frequency, where one-third of the application was applied every 4 h; and low frequency, where the same amount of irrigation water was applied without interruption during the same time period (Camp et al., 1993).

Because of the buried tube, we could not subsoil annually (the recommended practice for this soil). All plots had been subsoiled in August 1984. In November 1984, microirrigation tubes were plowed into the subsurface tube placement treatment using a steel tube attached to a subsoil shank as a guide. Hardpans reconsolidate in these soils to

root limiting strengths within a year after deep tillage by natural reconsolidation, traffic and disking (Busscher et al., 1986). All readings were taken in reconsolidated soil.

A surface irrigation tubing was installed in the plots each year after planting. They were removed before frost.

After the end of the bean harvest (July 15, 1988 and August 8, 1989), cone index readings were taken with the hand-held penetrometer. Data were taken and handled using the same method described earlier.

For both cotton and bean data, we analyzed cone index as a function of soil water content and other independent variables using the general linear model (GLM) ANOVA in SAS (SAS Institute, 1990). Cone index data were analyzed using a split–split plot randomized complete block design. In the cotton experiment, cover crop was the main treatment with splits on tillage, depth and date of measurement. For the bean experiment, tube placement and irrigation frequency were the main plots with splits on depth and date of measurement. For both data sets, water content was treated as a continuous covariate.

2.4. Corrections for water content

To reduce error mean squares, Eqs. (1)–(3) were fit after averaging cone indices and water contents over reps. Corrections were made separately for depth intervals and for treatments. Depths were gathered into two groups based on intervals that did not exhibit significant differences in the GLM ANOVA for the original data. These depth intervals were essentially the E and Bt horizons of the soils used in the experiments.

Parameters a and b were calculated for each depth interval or treatment by the method of least squares, using TableCurve. Comparisons were made between each treatment pair within experiments. Parameters were compared by calculating an approximate Z statistic for each parameter, a and b. Eqs. (1)–(3) were compared to one another using a simple F statistic. The $P \leq 0.05$ level of significance was used, unless otherwise specified.

Corrections of cone indices for differences of water content were based on a first term of a Taylor series expansion:

$$C_c = C_o + \frac{dC}{dW}(W_c - W_o) \tag{4}$$

where C_c was the corrected cone index, C_o was the original cone index, W_c was the common water content to which the cone indices were being corrected, W_o was the original water content of C_o, and dC/dW was the first derivative of any one of Eqs. (1)–(3). We chose W_c near the dryer end of the range of water contents. This kept $(W_c - W_o) > 0$ and prevented any calculated C_c from being less than zero. We chose the Taylor series type of correction, as opposed to a ratio, since it corrected cone indices based on differences of water content, which was the objective of this experiment. We reanalyzed corrected cone indices within GLM in the same manner as uncorrected cone indices listed above.

3. Results and discussion

3.1. The cotton experiment

Parameters a and b were calculated and compared for depths grouped by 0.25–0.35 m and 0.40–0.55 m, roughly the E and Bt horizons. Neither depth interval had significant coefficient of determination ($r^2 < 0.2$) for any of Eqs. (1)–(3). Several researchers have shown that the E horizon is growth-limiting based on high soil strength (Doty et al., 1975; Trouse and Reaves, 1980; Box and Langdale, 1984). We anticipated that horizons, where cone indices differ (Bauer and Busscher, 1996), would have an influence on the correction of cone index for water content. It did not. Depth difference was ignored and data were merged for other parameter calculations.

The difference between years had similar results. Relationships between cone index and water content for neither year had a significant coefficient of determination ($r^2 < 0.22$ for 1991 and $r^2 < 0.47$ for 1992). The difference between years was also ignored and data were merged for other parameter calculations.

We calculated separate parameters for Eqs. (1)–(3) for each of the four treatments: vetch winter cover-conventional tillage, vetch winter cover-conservation tillage, fallow winter cover-conventional tillage, and fallow winter cover-conservation tillage. Coefficients of determination ranged from 0.72 to 0.92 (Table 1, Fig. 1).

Table 1
Parameters for the cotton experiment calculated by the method of least squares

Treatment	Parameter			
	a	b	ems[a]	r^2
	Eq. (1)			
Fal-Conv[b]	0.693	−0.81	6.08	0.74[c]
Fal-Cons	0.634	−0.71	1.37	0.92[c]
Vetch-Conv	0.299	−1.12	5.12	0.89[c]
Vetch-Cons	1.50	−0.50	3.60	0.77[c]
	Eq. (2)			
Fal-Conv	10.7	8.12	6.32	0.72[c]
Fal-Cons	8.09	9.02	1.49	0.91[c]
Vetch-Conv	15.0	12.6	5.73	0.87[c]
Vetch-Cons	8.58	5.64	3.61	0.77[c]
	Eq. (3)			
Fal-Conv	11.1	−8.96	6.30	0.72[c]
Fal-Cons	8.31	−9.74	1.48	0.91[c]
Vetch-Conv	15.7	−13.8	5.66	0.87[c]
Vetch-Cons	8.76	−6.16	3.60	0.77[c]

[a] Error mean square.
[b] Fal-Conv: fallow conventional; Fal-Cons: fallow conservation; Vetch-Conv: vetch conventional; Vetch-Cons: vetch conservation. Number of data (n) after averaging over 4 reps: $n = 14$ for Fal-Conv, Fal-Cons, Vetch-Conv, and Vetch-Cons.
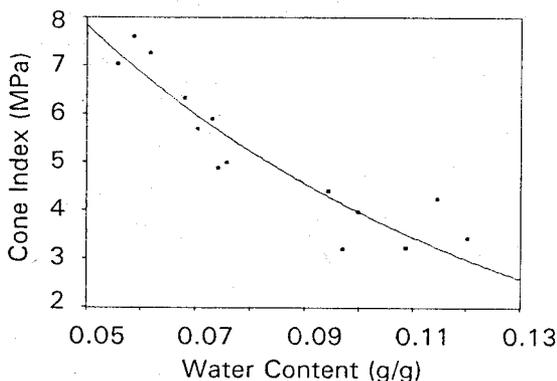[c] Significant at the $P \leq 0.01$ levels or less.

Fig. 1. Cone index vs. water content for vetch winter cover conservation tillage with Eq. (2) ($C = a(1 - W)^b$). Data were used to determine parameters a and b of Table 1 with the method of least squares.

We compared the parameters for the four treatments to one another. First, we compared vetch conservation tillage to fallow conservation tillage. Parameters a and b were significantly different at the $P \leq 0.01$ level. Second, we compared vetch conventional tillage to fallow conventional tillage. Here, b was significantly different at $P \leq 0.05$ for Eqs. (2) and (3). Parameter differences for cover crop treatments were unexpected since we ignored the upper 0.25 m of the profile. However, we observed less water ponded on cover crop plots during heavy rains. A deep cover crop effect could be the result of improved infiltration and reconsolidation within the vetch plots. Third, we compared vetch conservation tillage to vetch conventional tillage. Parameters a and b were significantly different at the $P \leq 0.01$ level of significance. Finally, we compared fallow conservation tillage to fallow conventional tillage where neither parameter a nor b was different.

We also calculated a set of parameters for all four treatments taken together. These parameters did not fit any of Eqs. (1)–(3) ($r^2 \sim 0.39$), as well as parameters for the individual treatments (Fig. 2).

Cone indices were corrected for water content with Eq. (4). Here, we used both a single-equation correction (one equation for all treatments taken together) and a multiple-equation correction (four equations with the separate parameters for each treatment, Table 1). Uncorrected and corrected cone indices were analyzed in GLM. The ANOVA for corrected cone indices was analyzed two ways, with and without the original water contents in the design. We used the design with water content to see if the cone index dependence on water content was reduced or eliminated. The design without the water content was the proper design after elimination of the water content as an independent variable. Both designs gave the same results, unless otherwise specified.

Before correction, cone index varied with water content in GLM with an F value of 19. We reanalyzed the data after a single-equation and a multiple-equation correction with water content in the ANOVA design. The F value was reduced for both cases (Table 2). Corrected cone indices generally reduced the model error mean squares (ems), which would increase the F value. However, water content ems were also reduced (Table 2). As a result, the F value and its effect on cone index were reduced. In one
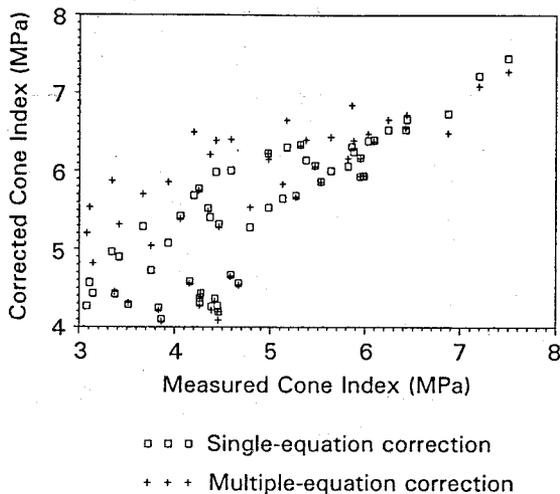
Fig. 2. Corrected vs. measured cone indices for all cotton data using Eq. (2) and parameters from Table 1.

instance, Eq. (1) with the multiple-equation correction, model ems increased. Here, the water content ems was lowest and F values were not significant. For the other equations, ems values were about the same. Both had lower F values than the uncorrected case showing reduced significance. Water content ems were lower for multiple-equation corrections than for single-equation corrections, presumably because multiple-equation corrections fit the data better.

Within the ANOVA of the uncorrected data, cone indices for winter cover and tillage treatments were not different. After correction, cone indices for winter cover were not different; cone indices for tillage treatments were different for the multiple-equation corrections of Eqs. (2) and (3) at $P \leq 0.01$ and 0.07, respectively (Table 3, both were $P \leq 0.04$ for the design without the water content). Water contents of conventional tillage (0.087 g/g with 0.029 standard deviation) and conservation tillage (0.074 g/g with 0.023 standard deviation) were corrected to 0.06 g/g. The greater correction for the conventional tillage led to the increased difference between the two and the significant difference. Cone indices for conventional tillage were higher than those for

Table 2

Uncorrected and corrected error mean squares (ems) and F values for the cotton experiment

Correction	Single-equation correction			Multiple-equation correction		
	F-value	Model ems	Water ems	F-value	Model ems	Water ems
none	19.2	0.0065	0.126	19.2	0.0065	0.126
Eq. (1)	2.33	0.0082	0.019	0.12	0.0110	0.001
Eq. (2)	5.12	0.0055	0.028	2.68	0.0056	0.015
Eq. (3)	5.17	0.0055	0.028	2.65	0.0056	0.015

Table 3
Mean cone indices: uncorrected and corrected for differences in water content for the cotton experiment

Equation	Single-equation correction				Multiple-equation correction			
	Vetch cover		Fallow		Vetch cover		Fallow	
	Conser-vation	Conven-tional	Conser-vation	Conven-tional	Conser-vation	Conven-tional	Conser-vation	Conven-tional
uncor-rected	5.21	4.87	4.16	4.82	5.21	4.87	4.16	4.82
Eq. (1)	5.74[a]	5.50	3.90	5.53	5.72	5.75	3.84	5.79
Eq. (2)	5.89	5.71	4.36	5.77	5.87	6.23	4.33	6.03
Eq. (3)	5.88	5.70	4.34	5.74	5.86	6.20	4.31	6.01

[a] Higher corrected cone indices reflect the lower water content used as a standard.
Values are expressed in MPa.

conservation tillage before (4.95 vs. 4.76 MPa) and after (6.22 vs. 5.14 MPa for Eq. (2)) multiple-equation correction.

If the single-equation correction was suitable, we could have stated that there were differences in the tillage treatment after correction that did not exist before, or that the water content differences before correction had masked treatment differences. However, since only the multiple-equation correction was meaningful, differences after correction may reflect real differences or may be a manifestation of the different corrections.

If we assume that the treatment differences after correction are real, higher cone indices for conventional tillage are reasonable. These plots were disked; conservation tillage plots were not.

3.2. The bean experiment

When parameters were analyzed for depth or year, bean data had results similar to cotton. Depth intervals did not have a significant relationship ($r^2 < 0.27$). Analysis by year had acceptable regressions ($r^2 = 0.61$–0.64 and ems = 6.06–6.22) but no significant differences. We ignored depth and year and merged data for other calculations.

We calculated separate parameters for Eqs. (1)–(3) for both high and low frequency irrigation and for both buried and surface microirrigation tube placement (Table 4). For irrigation frequency, no differences were found between parameters. For microirrigation tube placement, parameter b was different at $P \leq 0.05$ for all equations. The single-equation fit of all treatments was reasonable ($r^2 \sim 0.64$ and ems ~ 6.0).

Cone indices were corrected for water content (Eq. (4)) using parameters from different tube placement treatments, multiple-equation correction, and using the single-equation fit (Fig. 3). Corrected cone indices were reanalyzed in GLM in the same manner described earlier. Designs with and without water content gave the same results, unless otherwise stated.

Before correction, cone index varied with water content with an F value of 49. Single- and multiple-equation corrections reduced F values, especially for Eqs. (2) and (3) (Table 5). For the corrected cone indices, the model ems were reduced; the water

Table 4

Parameters for the bean experiment calculated by the method of least squares

Treatment	Parameter			
	a	b	ems[a]	r^2
	Eq. (1)			
Surface	0.088	−1.85	5.63	0.70[b]
Buried	0.242	−1.34	6.12	0.58[b]
Hi-frequency	0.210	−1.41	6.20	0.55[b]
Lo-frequency	0.106	−1.74	5.62	0.72[b]
	Eq. (2)			
Surface[c]	17.5	10.8	5.65	0.70[b]
Buried	11.4	7.99	6.07	0.59[b]
Hi-frequency	12.1	8.31	6.15	0.56[b]
Lo-frequency	15.9	10.4	5.60	0.72[b]
	Eq. (3)			
Surface	20.2	−12.7	5.64	0.70[b]
Buried	12.6	−9.36	6.07	0.59[b]
Hi-frequency	13.5	−9.77	6.15	0.56[b]
Lo-frequency	18.2	−12.2	5.60	0.72[b]

[a] Error mean square.

[b] Significant at the $P \le 0.01$ levels or less.

[c] Number of data (n) after averaging over 4 reps: $n = 54$ for Surface, Buried, Hi-, and Lo-frequency.

content ems were reduced even more. Reductions of F and ems were about the same for either single- or multiple-equation corrections (Table 5, Fig. 3).

In the ANOVA of uncorrected data, cone indices were not significantly different for tube placement or frequency of irrigation treatments. After either single- or multiple-

□ □ □ Single-equation correction

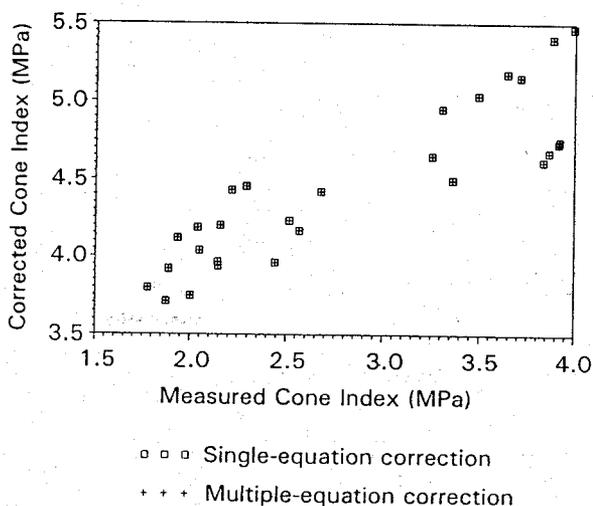+ + + Multiple-equation correction

Fig. 3. Corrected vs. measured cone indices for the green bean data using Eq. (2) and parameters from Table 3.

Table 5
Uncorrected and corrected error mean squares (ems) and F values for the bean experiment

Correction	One-equation correction			Two-equation correction		
	F-value	Model ems	Water ems	F-value	Model ems	Water ems
none	49.0	0.0205	1.01	49.0	0.0205	1.01
Eq. (1)	24.9	0.0088	0.22	25.4	0.0090	0.23
Eq. (2)	6.24	0.0086	0.054	6.62	0.0088	0.058
Eq. (3)	8.50	0.0086	0.073	9.04	0.0088	0.080

equation corrections, cone indices were different ($P \leq 0.01$) for tube placements (Table 6). For uncorrected values, cone indices of the buried treatment were greater than the surface treatment (2.90 vs. 2.72 MPa). For single- and multiple-equation corrections, cone indices for the surface treatment were greater than for the buried treatment (4.62 vs. 4.34 MPa using Eq. (3)).

The water contents of buried placement (0.15 g/g with 0.031 standard deviation) and surface placement (0.16 g/g with 0.027 standard deviation) were corrected to 0.10 g/g. The greater correction for the surface treatment led to its higher cone indices after correction and its significant difference.

Since the single-equation correction was suitable, cone index differences between the buried and surface treatments were masked by differences in water content before correction. The single-equation correction was about the same as the multiple-equation correction. Differences for tube placement could be a result of different reconsolidation caused by irrigation water entering the soil at the surface or in the subsurface.

3.3. Differences among the equations

In an attempt to improve the relationship between cone index and water content, we forced the cone index of the empirical relationship to go through zero at 40% water content. Forty percent is the approximate value of saturated water content. This was accomplished by adding a term $(0.4-W)$ to each of Eqs. (1)–(3). It did not improve the relationship. In fact, there were few differences between Eqs. (1)–(3) and these

Table 6
Mean cone indices: uncorrected and corrected for differences in water content for the green bean experiment

Equation	Single-equation correction				Multiple-equation correction			
	Tube placement		Irrigation frequency		Tube placement		Irrigation frequency	
	Buried	Surface	Hi	Lo	Buried	Surface	Hi	Lo
uncorrected	2.80	2.61	2.76	2.65	2.80	2.61	2.76	2.65
Eq. (1)	4.28[a]	4.15	4.27	4.16	4.12	4.36	4.30	4.18
Eq. (2)	4.43	4.35	4.46	4.32	4.27	4.56	4.49	4.34
Eq. (3)	4.41	4.32	4.44	4.30	4.25	4.52	4.45	4.31

[a]Higher corrected cone indices reflect the lower water content used as a standard.
Values are expressed in MPa.

equations. Furthermore, we compared all six equations to one another with simple F tests that used the ems of the various fits (data not shown; most $F \simeq 1$). No single equation was ever statistically better than another.

4. Conclusions

Significant differences between parameters were calculated for some different treatments. At times, different treatments require separate parameters to correct cone indices for water contents. Ley et al. (1993) reported similar results. They had different slopes for tensile strength vs. water content of different management treatments. The need for different equations for different treatments may account for the difficulty that researchers, such as Busscher (1990), had in developing this relationship in the past.

When corrections can be made with a single equation, corrected cone indices can be reinterpreted. Changes in cone index treatment significance as a result of the correction can be interpreted as having been masked by the differences in water content. When corrections require multiple equations, differences may be real or may be a manifestation of the correction differences. Multiple-equation corrections cannot guarantee that the differences are a result of the correction (unless some way to coordinate the equations and to assure a uniform correction can be found). In this case, water content can still be used as an independent variable in the GLM (Asady et al., 1987). But this assumes a linear relationship.

We found a few differences among the equations that were used to fit the data. Eqs. (2) and (3) showed differences between parameters for separate treatments when Eq. (1) did not. Further, corrected cone indices using Eqs. (2) and (3) showed differences among treatments in the ANOVAs of corrected cone indices when Eq. (1) did not.

Correction of cone index for water content led to a decreased significance of cone index dependence on water content within GLM analyses. This was true whether we used a one-equation correction of cone index for water content, or a more-than-one-equation correction based on treatments.

Correction of cone index for water content led to increased significance of treatment differences. If a one-equation correction was used, this difference had been masked by differences in water content before correction. If a multiple-correction equation was used, the difference may be real or a result of different corrections.

References

Asady, G.H., Hook, J.E., Threadgill, E.D., 1987. Tillage induced modifications of cone index and bulk density in a Coastal Plain soil. Agronomy Abstracts, p. 235.

Ayers, P.D., Perumpral, J.V., 1982. Moisture and density effect on cone index. Trans. ASAE 25 (5), 1169–1172.

Bauer, P.J., Busscher, W.J., 1996. Winter cover and tillage influences on Coastal Plain cotton production. J. Prod. Agric. 9 (1), 750–754.

Box, J.E., Langdale, G.W., 1984. The effects of in-row subsoil tillage on corn yields in the southeastern Coastal Plains of the United States. Soil Till. Res. 4, 67–78.

Bresson, L.M., Moran, C.J., 1995. Structural change induced by wetting and drying in seedbeds of a hardsetting soil with contrasting aggregate size distribution. Eur. J. Soil Sci. 46 (2), 205–214.

Busscher, W.J., 1990. Adjustment of flat-tipped penetrometer resistance data to a common water content. Trans. ASAE 33 (2), 519–524.

Busscher, W.J., Sojka, R.E., Doty, C.W., 1986. Residual effects of tillage on Coastal Plain soil strength. Soil Sci. 141, 144–148.

Busscher, W.J., Sojka, R.E., Sadler, E.J., Doty, C.W., 1985. Simplified data analysis for an inexpensive, manual analogue penetrometer. Conput. Elect. Agric. 1, 197–204.

Camp, C.R., Garrett, J.T., Sadler, E.J., Busscher, W.J., 1993. Microirrigation management for double-cropped vegetables in a humid area. Trans. ASAE 36 (6), 1639–1644.

Camp, C.R., Lund, Z.F., 1968. Effect of mechanical impedance on cotton root growth. Trans. ASAE 11 (2), 188–190.

Carter, L.M., 1967. Portable penetrometer measures soil strength profiles. Agric. Eng. 48, 348–349.

Doty, C.W., Campbell, R.B., Reicosky, D.C., 1975. Crop response to chiseling and irrigation in soils with a compact A2 horizon. Trans. ASAE 18 (4), 668–672.

Ley, G.J., Laryea, K.B., 1994. Spatial variability in penetration resistance of a hardsetting tropical alfisol. Soil Till. Res. 29 (4), 367–381.

Ley, G.J., Mullins, C.E., Lal, R., 1993. Effects of soil properties on the strength of weak structured tropical soils. Soil Till. Res. 28, 1–13.

Ley, G.J., Mullins, C.E., Lal, R., 1995. The potential restriction to root growth in structurally weak tropical soils. Soil Till. Res. 33 (2), 133–142.

Martino, D.L., Shaykewich, C.F., 1994. Root penetration profiles of wheat and barley as affected by soil penetration resistance in field conditions. Can. J. Soil Sci. 74 (2), 193–200.

Mielke, L.N., Powers, W.L., Badri, S., Jones, A.J., 1994. Estimating soil water content from soil strength. Soil Till. Res. 31, 199–209.

Mirreh, H.F., Ketcheson, J.W., 1972. Influence of bulk density and matric pressure to soil resistance to penetration. Can. J. Soil Sci. 52, 477–483.

Ohu, J.O., Raghavan, G.S.V., McKyes, E., 1988. Cone index prediction of compacted soils. Trans. ASAE 31 (2), 306–310.

Perumpral, J.V., 1987. Cone penetrometer application: A review. Trans. ASAE 30 (4), 939–944.

SAS Institute, 1990. SAS Language: Reference, Version 6. SAS Institute, SAS Circle, Box 8000, Cary. NC 27512-8000.

Spivey, L.D. Jr., Busscher, W.J., Campbell, R.B., 1986. The effect of texture on strength in southeastern Coastal Plain soils. Soil Till. Res. 6, 351–363.

Taylor, H.M., Gardner, H.R., 1963. Penetration of cotton seedling taproots as influenced by bulk density, moisture content, and strength of the soil. Soil Sci. 96, 153–156.

Tollner, E.W., Verma, B.P., 1987. Lubricated and nonlubricated cone penetrometer performance comparison in six soils. Trans. ASAE 30 (6), 1611–1618.

Trouse, A.C., Reaves, C.A., 1980. Reducing energy inputs into no-tillage systems. In: Gallaher, T.N. (Ed.), No-tillage Systems, 19 June 1980, Univ. of Florida, Gainesville, FL, p. 188–195.

Unger, P.W., Kaspar, T.C., 1994. Soil compaction and root growth — a review. Agron. J. 86 (5), 759–766.

Yasin, M., Grisso, R.D., Bashford, L.L., Jones, A.J., Mielke, L.N., 1993. Normalizing cone resistance values by covariance analysis. Trans. ASAE 36 (5), 1267–1270.