

EVALUATION OF PRESENT CONDITIONS
IN A WATER RESOURCE PROJECT

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SUMMARY: A section about 1,800 m wide and 4,000 m along Mitchell Creek in Edgecombe and Pitt Counties, North Carolina was studied over a 3-year period. The first two years, 1980-81, the area was studied as a drainage system. In 1982 a Fabridam was built to control the water level in the 2-3 m deep channels. Yield, water table elevations, stress day indices, and economical analysis are covered in this report.



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1 ABSTRACT

2 A section about 1800 m wide and 4000 m up Mitchell Creek in Edge-
3 combe and Pitt Counties, North Carolina, was studied over a 3-year
4 period. For the first two years , 1980-81, the deep channels in these
5 sandy soils showed a water table drawdown of about 3 m near the stream
6 which affected the water table 884 m away. Corn yields near the creek
7 were half those at 800 m from the creek. Stress day indices varied
8 inversely to the yield. In 1982 a Fabridam, a fabric dam filled with
9 water that automatically controls water levels in the creek and allows
10 floods to pass, was installed on Mitchell Creek. After the Fabridam
11 was installed, the water table in the fields above the dam rose signif-
12 icantly. Corn yields were increased by 25% within 488 m of Mitchell
13 Creek where the water level in the stream was controlled. This increase
14 in yield would pay for the structure over a period of 15 years.

15 INTRODUCTION

16 There are about 15-25 million hectares of drained farm land in the
17 humid region of the U.S. About 3.4 million hectares of sandy, sandy
18 loam, and organic soils are found in the South Atlantic Coastal Plain
19 of North Carolina, South Carolina, Georgia, Florida, and Alabama (Wen-
20 berg and Gerald, 1982). It is estimated from discussions with Soil
21 Conservation Service personnel that there are another 1.5 million
22 hectares of these soils in Virginia, Maryland, Delaware, and New Jersey.

23 When the water table is greater than 1.5 m from the surface, the
24 water-holding capacities of these sandy soils is about 3 cm/30cm of
25 soil or less; enough to supply crop water needs for 4 to 7 days. The
26 low water-holding capacity of these sandy soils makes them susceptible
27 to becoming droughty when the water table is drained too far below the

1 soil surface. However, artificial drainage is necessary for traffic-
2 ability in the spring and fall and to protect crops from excessive
3 soil water conditions during wet periods. Improved drainage channels
4 are also needed for flood protection.

5 Controlling the stream water levels is considered to be a system
6 of control drainage, subirrigation or total water management system.
7 French scientists, Bordas and Mathieu (1931) reported higher yields
8 from a controlled water table than from other irrigation systems.
9 Some practical aspects of controlled subsurface drainage were considered
10 by Morris (1949) who concluded that in the future all artificial
11 drainage may be controlled drainage.

12 Kalisvaart (1958) reported on controlling stream water levels for
13 subirrigation in the Zuiderzee Poldus in the Netherlands where only
14 agricultural land with low water-holding capacities needed irrigation.
15 In portions of this land, water can be supplied by subirrigation which
16 might be termed "drainage in reverse". He pointed out that in fields
17 where the subsoil consisted of deep and very permeable low terrace
18 sands, "as a rule subirrigation (reversible drainage) will be the most
19 suitable method" for irrigation.

20 In the United States, most data on control drainage and sub-
21 irrigation must be gleaned from drainage research. For example, we
22 find in Table 2.2, pages 34 and 35 of Wessling (1974) that in 21 of
23 the 35 cases reported, yields decreased when the water table was
24 maintained below certain levels from the surface. Water table depth
25 for maximum yields varied with crops and soil classifications. However,
26 for all soils classified as loams, sandy loam, and loamy fine sands,
27 he showed that there was a minimum water table depth that produced

1 maximum yields, but for any greater depth to the water tables, yields
2 were reduced.

3 When the water table in sands, sandy loams, and silty clay loam
4 soils rose from 80 to 15 cm below the surface, corn yields decreased
5 from 100 to 45% of maximum yield, respectively. Likewise, when the
6 water table fell from 80 to 100 cm below the surface, corn yields
7 decreased from 100 to 45% of maximum, respectively. Soybean growing
8 on sandy loam soils were similarly affected. Yields for wheat, oats,
9 and barley growing on clay soil were somewhat similar for a rise in
10 water table, but 100% of maximum yield was reached at a water table
11 depth of 150 cm. Vegetable crop yields followed about the same trends
12 (Wesseling 1974). The fact that there were no yield decreases as the
13 water table receded in clay soils indicated that water-holding capacities
14 of the clay soils (6.4 cm/30 cm of soil) are higher than in sandy
15 soils (1.5 to 5 cm/30 cm of soil) (Turner et al., 1971).

16 In the Mid-Atlantic Coastal Plain, soils that are too dry during
17 one period may be excessively wet during another as a result of erratic
18 rainfall distribution and soil conditions. Drainage is needed during
19 periods of excessive rainfall, but when sandy soils are drained too
20 rapidly or deeply, drought stress will occur if it doesn't rain again
21 in 4 to 7 days (Doty, 1975b; Reicosky et al., 1976). An example of
22 this condition is the Conetoe Drainage District in North Carolina
23 where 26,000 hectares of land are drained in Public Law 566 drainage
24 project constructed in 1967. Several thousand hectares of cropland
25 that once were flooded several times a year are now protected. However,
26 to drain parts of the district, channels over 2 m deep were necessary.
27 Although flooding is no longer a problem, overdrainage near the channels

1 is believed to increase drought stresses and reduce yields. Farmers
2 are investing in irrigation systems, and domestic use well points are
3 being lowered to compensate for the lowered water table. Problems are
4 developing because of a lack of water to supply the ever growing
5 number of irrigation systems along the streams.

6 Control of the variation in the stream water level during non-flood
7 stages and the fast removal of flood flows are being studied. This
8 project, located in Pitt and Edgecombe Counties, North Carolina, is
9 the composite cooperative effort of agencies from the U.S. Department
10 of Agriculture, the Agricultural Research Service and the Soil Conserva-
11 tion Service; the North Carolina Agricultural Research Service, Depart-
12 ments of Biological and Agricultural Engineering and Soil Science, N.
13 C. State University; the drainage industry, Advance Drainage Systems,
14 Inc., and Hancor, Inc.; the Edgecome County Drainage District #2; and
15 local farmers and landowners.

16 The general objective of this research is to evaluate present
17 methods for design and operation of water table management systems and
18 to develop field-derived criteria to modify these systems for economic
19 efficiencies for water resource projects. This paper will (1) evaluate
20 the effects of deep ditches on field water table levels in sandy soil
21 and (2) give preliminary results on controlling the stream water
22 levels with a "Fabridam" on field water table levels and corn yields.

23 PROJECT DESCRIPTION AND PROCEDURE

24 The water management study is located on a 2-mile section of
25 Mitchell Creek (Fig. 2). The area, about 800 hectares, is flat to
26 gently rolling with no more than a 1.5-m difference in elevation. The
27 soil series Altavista, Augusta, Cape Fear, Conetoe, Portsmouth, Roanoke,

1 State, Tarboro, and Wahee were mapped and rechecked for each yield
2 sample site by the Soil Conservation Service. The soils are poorly to
3 somewhat excessively drained, formed in sandy fluvial and marine
4 sediments. They are underlain by a coarse sandy aquifer at about
5 1.5-m depth. The coarse sand is underlain by a layer of blue consistent
6 clay ranging in depth from 4 to 8 m below the surface. This clay
7 layer was found to be impermeable at points where it was measured, but
8 fissures may occur in the layer.

9 Six lines of water table observation wells were installed to
10 transect the area on each side of the creek. Well locations ranged
11 from 10 to 970 m from the channel in lines perpendicular to the creek
12 (Fig. 2). Forty wells were equipped with stage recorders and 22 were
13 read manually each week. There were 12 stream gaging sites equipped
14 with stage recorders, 7 on Mitchell Creek, 3 on intersecting channels,
15 and 2 on channels paralleling Mitchell Creek. Manual flow measurements
16 were made at 5 of these sites about twice weekly. Other sites were
17 measured about once a month. Hydraulic conductivity was measured with
18 a drill rig at random over the area.

19 A Fabridam-type structure (2.7 m high) (Fig. 3) was installed and
20 put into operation on 2 April 1982 across Mitchell Creek about midway
21 in the 3.5-km study area. The water inflatable fabric dam is about 6
22 m wide at the bottom of the creek bed and 13 m wide at bank height,
23 and is used to automatically control the water level in the creek
24 upstream. The Fabridam is capable of collapsing during flooding which
25 allows the channel to return to normal size. It can control the water
26 level in the channel to a depth of 2.45 m. For example, if the control
27 level is set at 11.45 m above MSL and a flood raises the upstream

1 level to 11.60 (0.15 m rise), the Fabridam begins to deflate, but will
2 remain controlled between 11.45 and 11.60 m. If the flood level still
3 rises to 11.62 m (0.17 m rise) another valve opens and the Fabridam
4 deflates faster, but automatic controls keep it between 11.45 and
5 11.60 m. If the flood continues to exist and the upstream water level
6 reaches 11.65 m (0.2 m rise), a 20.3-cm syphon will deflate the Fabridam
7 at a rate of about 0.06 m/min until there is no restriction in the
8 channel. As soon as the flood passes and the syphon breaks, the
9 Fabridam will be inflated to the original setting of 11.45 m.

10 Corn yields were sampled by hand from two replications near the
11 water table observation wells (Fig. 2). For this report the yields
12 are reported in two ways: (a) The distance from the channel to the
13 sample site was divided into seven sections, 0-50 m, 51-100 m, 101-200
14 m, 201-400 m, 401-600 m, 601-800 m, and greater than 800 m for the
15 data before the Fabridam (1980 and 1981). (b) After the fabridam was
16 installed in 1982, the yields were separated into treatments (1) no
17 water level control with and without irrigation and (2) water table
18 control by the Fabridam with and without irrigation. For the 1982
19 corn yield data, the nonirrigated data was divided into seven sections,
20 0-50 m, 51-100 m, 101-200 m, 201-300 m, 301-400 m, 401-500 m and
21 greater than 500 m the distance the channel to the sample site.
22 Average yields were regressed against distance from the channel for
23 before and after Fabridam installation. The 95% confidence limits on
24 all data was based on all sample sites, not just on the averaged data
25 (Eq.9.13, Steel and Torrie, 1960).

26 The stress-day index (SDI) were determined for each site where
27 corn yields were measured. The stress-day index is defined by:

$$SDI = \sum_{i=1}^n \left(1 - \frac{ET_i}{(SPE_i)(Kc_i)} \right) \quad [1]$$

where:

ET_i = calculated evapotranspiration for day i

SPE_i = screen pan evaporation for day i

Kc_i = crop factor Kc (Soil Conservation Service 1967)

The daily evapotranspiration (ET_i), which depends on the soil moisture conditions, is calculated by:

$$ET_i = \left\{ \begin{array}{ll} (SPE_i)(Kc_i) & , AW_{i-1} + F_i \geq (SPE_i)(Kc_i) \\ AW_{i-1} + F_i & , AW_{i-1} + F_i < (SPE_i)(Kc_i) \end{array} \right\} \quad [2]$$

The potential available water in the root zone (AWP_i) is calculated from the water balance equations.

$$AWP_i = AW_{i-1} + R_i + F_i - Et_i \quad [3]$$

where

AWP_i = potential available water in the root zone
for day i

AW_{i-1} = available water in the root zone for day $i-1$

R_i = rainfall for day i

F_i = upward flux of water into the root zone calculated from the soil water characteristic curve assuming steady state flux (Skaggs, 1981). In some cases, it was necessary to extrapolate F_i past the depth for which samples for soil water characteristics were taken. For example, near the channel, the water table position was greater than 2.0 m from the surface.

ET_i = evapotranspiration for day i from equation 2

1 The surplus water, (S_i), (runoff, lateral loss, and deep seepage) for
 2 day i is then defined by

$$3 \quad S_i = \left\{ \begin{array}{l} 0, AWP_i \leq MAW_i \\ AWP_i - MAW_i, AWP_i > MAW_i \end{array} \right\} \quad [4]$$

7 MAW_i = Maximum available water in the root zone based on
 8 the soil water characteristic which is a function
 9 of the soil type, the water table position and
 10 the rooting depth. Since the rooting depth and
 11 the water table position changes throughout the
 12 growing season, the amount of MAW_i is changing
 13 daily.

14 Therefore, the available water in the root zone (AW_i) for day i is
 15 then calculated as $AWP_i - S_i$ and

$$16 \quad AW_i = AW_{i-1} + R_i + F_i - S_i - ET_i \quad [5]$$

17 The available water in the root zone (AW_{i-1}) where i is the
 18 planting day is assumed to be MAW_i ; which is obtained from the soil
 19 water characteristics curve.

20 RESULTS AND DISCUSSION

21 Effect of Deep Ditches

22 Data were collected in 1980 and 1981 without water level controls
 23 to determine the effect of deep ditch drainage on the water table and
 24 crop yield. The 2-4 m deep channels are excellent for drainage and
 25 flood control, but frequently cause overdrainage in these deep sandy
 26 soils after the flood passes. Figure 4a shows the maximum and minimum
 27 water table elevations on each side of Mitchell Creek for well line

1 No. 5. The gradient towards the channel on the water table surface
2 extends to the measured distance of 884 m on the right side looking
3 downstream and to 696 m on the left side. The water table slope
4 towards the channel is greater for the first 400 m. Similar slopes of
5 the water table occur about 1200 m upstream at well line No. 3 (Fig.
6 4b) where the soil surface is relatively flat. This indicates that
7 water is being drained from the water table by Mitchell Creek at a
8 distance of at least 884 m. Assume that a maximum water table elevation
9 of about 12 m, (1 to 1.5 m below the surface) is the water table depth
10 at which corn can be grown without aeration problems (Wessling 1974,
11 See Fig. 1, and Benz et al. 1981). Then in these fields, the difference
12 from 12.0 m above MSL to the lowest water table elevations on 17
13 December 1981 is the amount of drop in the water table and overdrainage
14 near the channel caused by dry weather conditions and deep channels in
15 sandy soils along Mitchell Creek in 1980-81 (Fig. 4a, 4b).

16 The drop in the water table due to weather conditions and over-
17 drainage near the channel are shown with time for well line No. 5
18 (Fig. 5). At the beginning of data collection in 1980, the water
19 table elevation was about 11.5 m at 594 m from the creek, which is
20 lower than the elevation at which the water table should be maintained
21 without reducing yield (1.5 m below the surface). The water table
22 continued to drop through the remainder of 1980 and 1981, the minimum
23 elevation being about 10.7 m (1.3 m below the desired 12 m). A well
24 18 m from Mitchell Creek was at least 2.4 m below the desired water
25 level of about 1 m below the surface throughout 1980 and 1981.
26 The elevation of the water level in the creek was less than 9.6 m at
27 least 2.4 m below the desired 12-m elevation throughout 1980 and 1981.

1 Similar results were shown at well line No. 3 about 1200 m upstream.
2 The hydraulic conductivity of the surface 0-1.2 m ranged from 0.07 to
3 9.5 m/day, from 1.2 to 2.1 m from the surface ranged from 0.11 to 42.7
4 m/day, and 2.1 to 7.5 m from the surface ranged from 0.0 to 58.0 m/day
5 according to the depths of the blue clay layer. This indicates that
6 without water level control in the stream, these sandy soils with high
7 hydraulic conductivity are overdrained.

8 Stress Day Index and Corn Yield

9 The average stress day indices for the corn growing season for
10 each sample site where corn yield samples were taken in 1980 and 1981
11 was plotted against the average distance from Mitchell Creek (Fig.
12 6a). Stress, as indicated by stress day index, is related to the
13 distance from Mitchell Creek. Near the creek there were about 70 days
14 during the growing season when full ET for the corn crop was not
15 available, but at 700 m from Mitchell Creek there was less than 20
16 days that full ET was not supplied. This was because the water table
17 near the creek was drawn down to low by the deep drainage channel. At
18 700 m from the creek the water table was not so far from the surface
19 (Fig. 4a, 4b).

20 The relationship of corn yield to the distance the sample site
21 was away from Mitchell Creek shows that corn yields increased with
22 distance from the creek (Fig. 6b). Corn yields of 4.8 t/ha were
23 measured at 25 m from Mitchell Creek and increased at a rate of 0.1
24 t/ha for each 18.7 m (1 bu/38 ft) farther away from the creek to 9.0
25 t/ha at a distance of 810 m from Mitchell Creek. The yield-distance
26 relationship is the inverse to the SDI-distance relationship showing
27 that the corn crop for 1980 and 1981 growing seasons had more drought

1 stress (SDI = 70) and lower yields (4.8 t/ha) where the water table
2 was farther from the surface near Mitchell Creek (Fig. 4a, 4b). There
3 was considerably less drought stress (SDI = 11) and higher yields (8.6
4 t/ha) at 800 m from Mitchell Creek where the water table was closer to
5 the soil surface and water could reach the root system of the corn
6 plants. This shows the effects of overdrainage in these sandy soils
7 by the deep ditch systems required for flood control.

8 The data for the 1980 and 1981 corn-growing seasons show an
9 excellent linear relation ($R^2 = .99$) between the measured yields and the
10 calculated stress-day index based on screened-pan evaporation, soil
11 water characteristics, and water table depth (Fig. 7). With a SDI of
12 11, the average corn grain yield was only 4.8 t/ha. This is a 79%
13 increase in grain yield for an 84% decrease in SDI. Water table
14 levels varied over the two-year period, but the maximum and minimum
15 water table depth for a SID of 11, 8.6 t/ha corn yield, was between
16 1.4 and 0.8 m. (Fig. 4). This is in the range of the water table
17 depth that produced the best corn yield, 6.6 t/ha, as reported by Benz
18 et al., 1978. The maximum and minimum water table depth for a SDI of
19 70, 4.8 t/ha corn yield, was between 2.8 and 2.5 m from the surface
20 (Fig. 4). This corresponds to Benz et al., (1978) deep water table
21 data which produced 3.0 t/ha of corn grain. Doty et al. (1975a)
22 showed that corn silage yields increased by 1.1 t/ha for each additional
23 day the water table was 1.07 m or less from the surface. The water
24 table is being lowered to a point where the root system cannot extract
25 any water from the capillary zone above the water table. Overdrainage
26 occurring in these low water-holding capacity sandy soils with deep
27 channelization can be corrected by controlling water tables at less

1 than a 1.5-m depth. Two possible alternatives are: (1) drainage
2 channels should be less than 1.5 m deep, which can fill with debris
3 and cause flooding, and (2) automatic control structures must be
4 provided to control the water table level on channels large and deep
5 enough to handle flood flows. In either case, the drains would not
6 drain the land far away from the channel, and additional field drains
7 would be required to provide good water management.

8 Effects of Deep Channels with Water Level Controls

9 The Fabridam installation (Fig. 3) was completed on 2 April 1982
10 with the water level in the stream controlled at 10.67 m above MSL
11 until June 18 when the level was raised to 11.28 m. The control level
12 was raised to 11.55 m on July 6 and remained there for the rest of the
13 season. Several large rainfall events caused fluctuation in the dam,
14 but the floods passed easily. One 80 mm rain on August 11-12, 1982,
15 caused the Fabridam to operate seven times.

16 Corn requires the greatest amount of water from silking to ear
17 fill stages. The last of June (June 30) is considered to be a high
18 water use period for corn for both 1981 and 1982 at the research site.
19 The water table elevations for 30 June 1981 without water level control
20 and 30 June 1982 with Fabridam water level control are shown in Fig.
21 8a for well line 5, about 90 m upstream from the Fabridam. Near the
22 stream the water table was about 1.5 m closer to the surface in 1982
23 than in 1981. At about 200 m on either side of the channel the water
24 table was about 0.5 m closer to the surface in 1982 than in 1981. The
25 water table would have been slightly higher in 1982 than in 1981
26 without the Fabridam due to rainfall. Essentially, controlling the
27 water level in Mitchell Creek produced an almost flat water table with

1 variations in depth to the water table being the change in soil surface
2 elevation (Fig. 8a). Similar results were found about 1200 m upstream
3 from the Fabridam. Doty (1980) showed that corn received ample water
4 for good production with the water table less than 1.4 m from the
5 surface in a Goldsboro sandy clay loam soil in South Carolina.

6 Below the Fabridam, the stream remained at about its normal level
7 since there was no water table control (Fig. 8b). The general water
8 table was higher in 1982 than in 1981 due to rainfall. The water
9 table for 30 June 1982 paralleled that for 30 June 1981. Nearer the
10 stream, the water table was from about 2.4 to 3.7 m from the surface
11 while at distances between 500 and 700 m from Mitchell Creek, the
12 water table was from about 1.5 to 2.5 m from the surface. The water
13 table being closer to the surface at 500 to 700 m from Mitchell Creek
14 than near the Creek would suggest that crop yields should increase in
15 proportion to distance away from Mitchell Creek in the area without
16 water level control by the Fabridam (Fig. 8b). While in the area
17 where the water level in Mitchell Creek was controlled by the Fabridam,
18 the water table was essentially flat (Fig. 8a).

19 20 Corn Yield vs. Distance From Channel

21 The data for 1982 was the first yield results with water level
22 control in the channel. Data was collected from above the Fabridam
23 where the water level was controlled and below the structure without
24 water level control. The average corn yields from the four water
25 management systems are compared in Table 1. Without irrigation, the
26 system with water level control produced 16% more corn than the check
27 without control. With irrigation, 6.3 cm, the system with the water

1 level control produced 25% more corn than the check. Irrigation
2 applied to the system without water level control (check) produced 16%
3 more yield. However, the farmers in the area were applying the water,
4 and the application times were not the same. The water table was
5 about 1.5 m to 2.2 m from the surface on the water level control
6 system. Benz et al. (1978) showed an increase in yield from irrigation
7 when the water table was greater than 1.8 m from the surface.

8 Without water level control in the channel, yields increased with
9 distance away from Mitchell Creek (Fig. 9a). The linear regression
10 line had a slope of 0.007. This compares to a slope of 0.005 for the
11 1980-81 data (Fig. 6b). Even though 1982 was an excellent corn pro-
12 ducing year without water level control, about 5 t/ha (80 bu/A) of
13 grain was produced near the channel with the water table about 2.7 m
14 from the surface. At 550 m from the Mitchell Creek, 8.4 t/ha (134
15 bu/A) of corn was produced with a water table 1.7 m from the surface.
16 On a Hecla sandy loam soil in North Dakota, Follett et al. (1974)
17 reported average corn yields of 4.5 t/ha where the water table was
18 from 1.9 m to 2.9 m and 8.4 t/ha where the water table ranged from 0.7
19 m to 1.9 m for the two-year period of study. This shows the need for
20 water level control in the channel on these sandy soils.

21 Above the Fabridam where the water level was controlled, the
22 story was different. There was no increase in yield due to distance
23 from Mitchell Creek (Fig. 9b). The mean yield from 0 to 330 m from
24 Mitchell Creek was 8.3 t/ha (134 bu/A), almost the same as without
25 water level control at 550 m from the Creek. This shows that water
26 level control by the Fabridam increased yields near the deep channels.
27 In addition, flooding was controlled with up to 80 mm of rainfall.

1 There was some evidence of wet soils in the watershed caused by
2 controlling the water table. Two well sites in low elevations showed
3 that water table less than 0.7 m from the surface for 2- to 3-day
4 periods, and yields may have been reduced due to too wet conditions.
5 The only complaint about surface water was related to a clogged surface
6 outlet into a drainage ditch. After the outlet was cleared, the
7 ponded water drained. The water table was greater than 1 m below the
8 soil surface.

9 Stress Day Index After Fabridam

10 The SDI for the 1982 corn yield sample sites below the Fabridam,
11 without water level control, were regressed against distance from
12 Mitchell Creek (Fig. 10a). Although the regression coefficient ($R^2 =$
13 0.30) was low, the 1982 SDI-distance relationship was inverse to the
14 1982 yield-distance relationship (Fig. 9a). This inverse relationship
15 was similar to the one shown for the 1980-81 data (Fig. 6a,b). For
16 the 1982 corn yield sample sites above the Fabridam where the water
17 level in the stream was controlled, the SDI decreased also with distance
18 from the creek (Fig. 10b). However, the point at 330 m from the creek
19 is questionable. The soil series in the general area is mapped Cape
20 Fear and the closest point where the soil series had been determined
21 previously was the Portsmouth silt loam. The Portsmouth silt loam
22 soil water characteristic was used to determine SDI. The SDI for the
23 point at 330 m from the creek was also calculated with the soil water
24 characteristic of a Portsmouth coarse loamy variant soil which gave an
25 SDI of 32.08. With the Portsmouth coarse loamy variant series, there
26 would be no relationship between SDI and distance from the creek for
27 the yield plots above the Fabridam.

Stress Day Index Vs. Yield

All data points for 1980 through 1982 were used to give a relationship between SDI and measured yield (Fig. 11). The maximum single well site yield measured in the area was 10.52 t/ha for nonirrigated soils and 12.221 irrigated soils in 1982; 10.025 nonirrigated and 11.869 irrigated in 1980 and 1981. The maximum projected yield from the regression line (Fig. 10) shows that with a SDI of 0.0, the yield should be 10.554 t/ha, \pm 2.00 t/ha (168 bu/A) or from 8.5 to 12.5 t/ha for the 95% confidence limits. This compares favorably with the highest observed yield of 10.700 t/ha (170 bu/A) or the projected potential yield of 11.1 t/ha (177 bu/A) for the Tidewater Research Station, near Plymouth, North Carolina, about 100 miles east of this site (Hardjoamidjojo and Skaggs, 1982). However, our data show that plant populations are in the range of 37,000 to 57,000 plants/ha for nonirrigated fields and 49,000 to 72,000 plants/ha in the irrigated fields. North Carolina State University recommends 54,000 to 69,000 plants/ha for nonirrigated corn. Rhoads (1982) showed yields of 14.5 t/ha (230 bu/A) under irrigation at 90,000 plants/ha on a sandy soil in Florida. Therefore, when farmers use higher plant populations, yields should increase.

The low R^2 value indicating a wide scatter of points between corn yield and stress day index (Fig. 10) shows that some improvement is needed in obtaining stress day index. We plan to include some work by Hardjoamidjojo and Skaggs (1982) and include crop susceptibility factors, planting delay, and wet soil conditions for future studies on these data.

Economical Analysis of Water Table Control

1 to control the water table levels. The water level in the stream at
2 an elevation of 11.25 m, about 1 to 2 m from the soil surface was
3 relatively flat with the variation in depth of the water table similar
4 to the variation in soil surface elevation. On the average, the water
5 table in the area was about 0.65 m higher after the stream water level
6 was raised about 1.25 m.

7 Measurement of water table levels below the Fabridam showed the
8 water table elevations to be about 0.2 m higher than they were in 1981
9 due to rainfall, but were drawn down sharply near the channel.

10 Corn yields were affected by the stream water level control and
11 the higher water tables. Nonirrigated corn yields above the Fabridam
12 were 16% greater than those from below the Fabridam. Irrigated yields
13 were 25% higher than those from below the Fabridam.

14 The method of calculating SDI can use some improvement. This is
15 indicated by the fact that SDI was more closely related to yield in
16 the drier years of 1980 and 1981 (Fig. 7) when the rainfall was more
17 scattered than in 1982, a year of more abundant rainfall (Fig. 10a,
18 b). However, the SDI did a good job in projecting the maximum yield
19 of 10.554 t/ha (168 bu/A).

20 Farmers and action agency personnel are very interested in the
21 economical analysis of this project. Based on 1982 data only, the use
22 of the Fabridam, without additional irrigation equipment, should pay
23 for itself in 15 years at 10% interest. This would leave \$5,300 per
24 year for maintenance and management. However, with irrigation, the
25 Fabridam will pay for itself in 15 years and leave \$214,700 (\$14,300/yr)
26 additional for maintenance and management.

27 Overdrainage is occurring in the low water-holding capacity sandy

1 soils with high hydraulic conductivities and deep channelization
2 throughout the Southeast. Shallow channels would probably decrease
3 overdrainage, but maintenance, flood control, and proper drainage
4 during wet periods are problems that would still exist. Engineering
5 design criteria must be established for future planning of water
6 resource projects that will provide proper drainage and flood control
7 during wet periods and still provide soil water storage in the soil
8 profile and in the stream channels for supplying water for crop needs
9 either by capillary rise in the soil or by being available for irrigation
10 pumping.

11 Design of water level control structures can be critical in
12 streams subject to flooding. These structures must be automatic in
13 order to pass flood water. We have shown the possible economic effects
14 of the better and more expensive water level control structure, the
15 Fabridam, but our limited data show it to be worthwhile. Why take the
16 chance of designing a water level control structure that man has to
17 operate and risk loss of property and possibly life. Design all water
18 level control structures to operate automatically.

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Table 1. Corn yield data for the four water management systems on Mitchell Creek for 1982.

Table 2. Present value of the 1982 corn crop at \$98.40/ton (\$2.50/bu) projected for 15 years at 10% interest (PWf = 7.606).

Table 1. Corn yield data for the four water management systems on Mitchell Creek for 1982.

Water Management System	Mean Corn Yield	
	Nonirrigated	Irrigated
	-----t/ha-----	
No Water Level Control	7.157 b*	8.289 b
Control by Fabridam	8.321 b	10.326 a

* Yield followed by the same letter are not significantly different by DMRT at 5%.

Table 2. Present value of the 1982 corn crop at \$98.40/ton (\$2.50/bu) projected for 15 years at 10% interest (PWF = 7.606). The estimated life of the fabriadam is 50 years.

Treatment	Yield ^{1/} (t/ha)	Area involved (ha)	Present value of crop	Increase value due to treatment	Present cost of treatment (Fabriadam)	Returns for maintenance- management
No controls	6.68	202	1,009,900	-		1,009,900
Fabriadam control	8.36	202	1,263,900	254,000	248,700	1,015,200
Fabriadam plus irrigation	10.33	142	1,473,300	463,400	248,700	1,224,600

-----dollars-----

^{1/} Average yields for 0 to 488 m from Mitchell Creek (Fig. 9a,b)

^{2/} This 142-ha area had a yield increase of 1.97 t/ha because irrigation water could be supplied. Therefore, the present value also includes the present value of the 202 ha with water level control by the Fabriadam. It was also assumed that the farmer owned the irrigation system.

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3 by a Fabridam.

4 Fig. 10. Relation of average stress-day index to distance from Mitchell
5 Creek (a) with no water level control and (b) with water
6 level control by the Fabridam.

7 Fig. 11. Stress-day index vs. corn yield for three growing seasons,
8 1980, 1981, and 1982.

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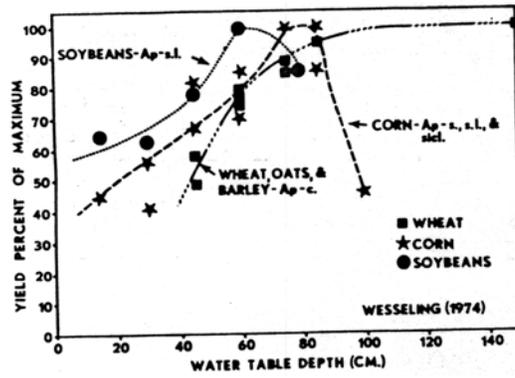


Fig. 1. Water table depth vs. percent of maximum yield for major field crops (after Wesseling 1974).

Original picture will be used for this figure

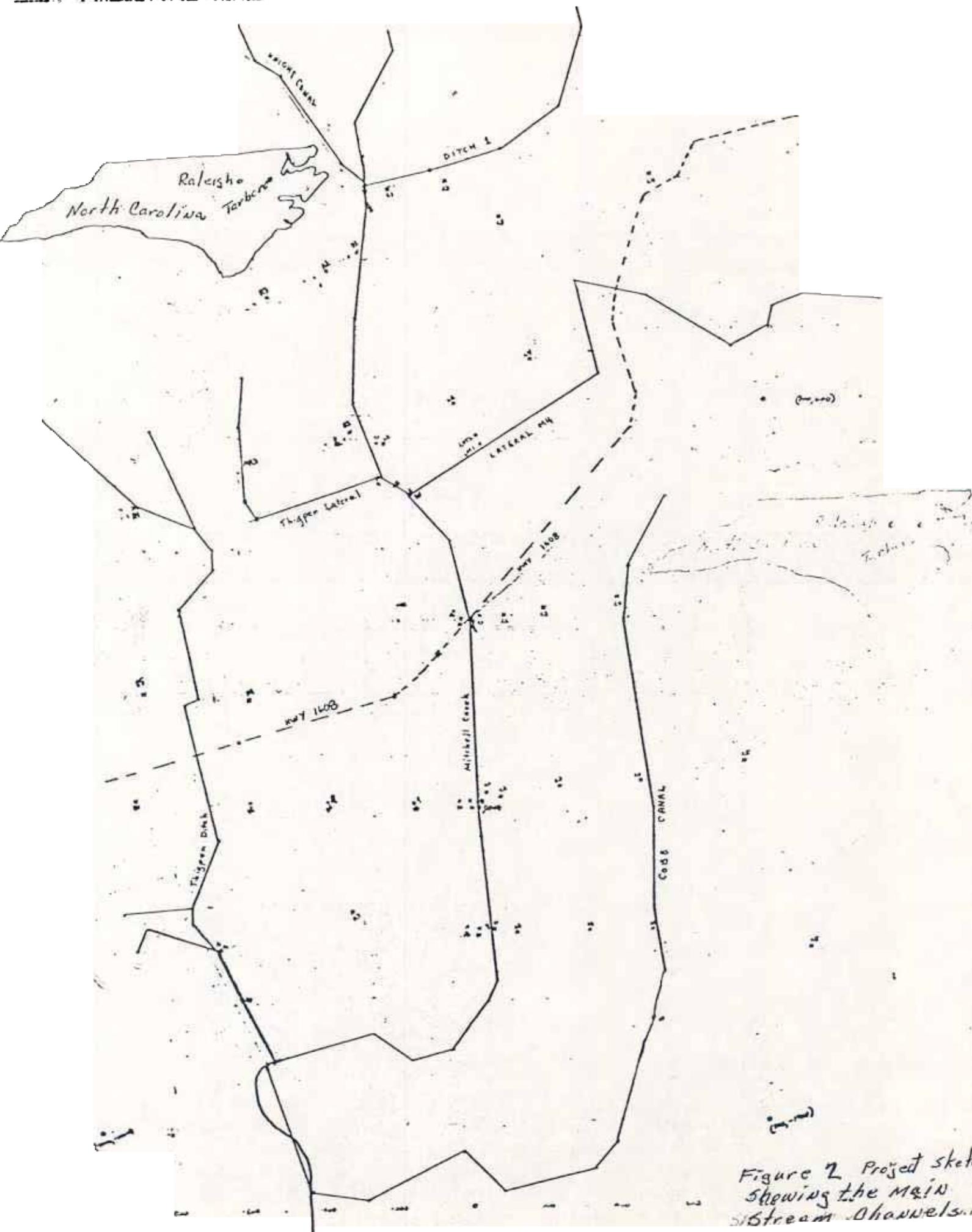


Figure 2 Project sketch showing the main stream channels.

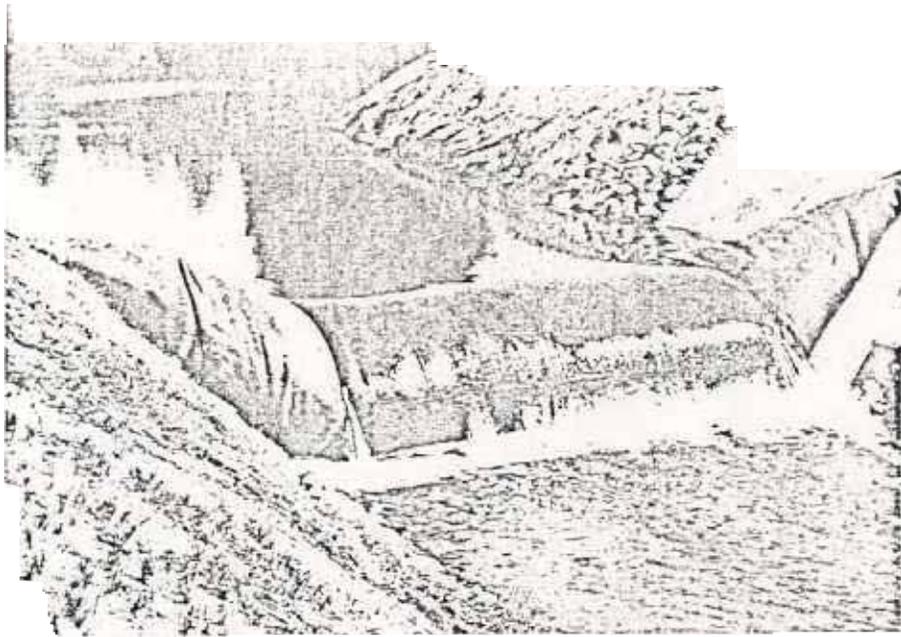
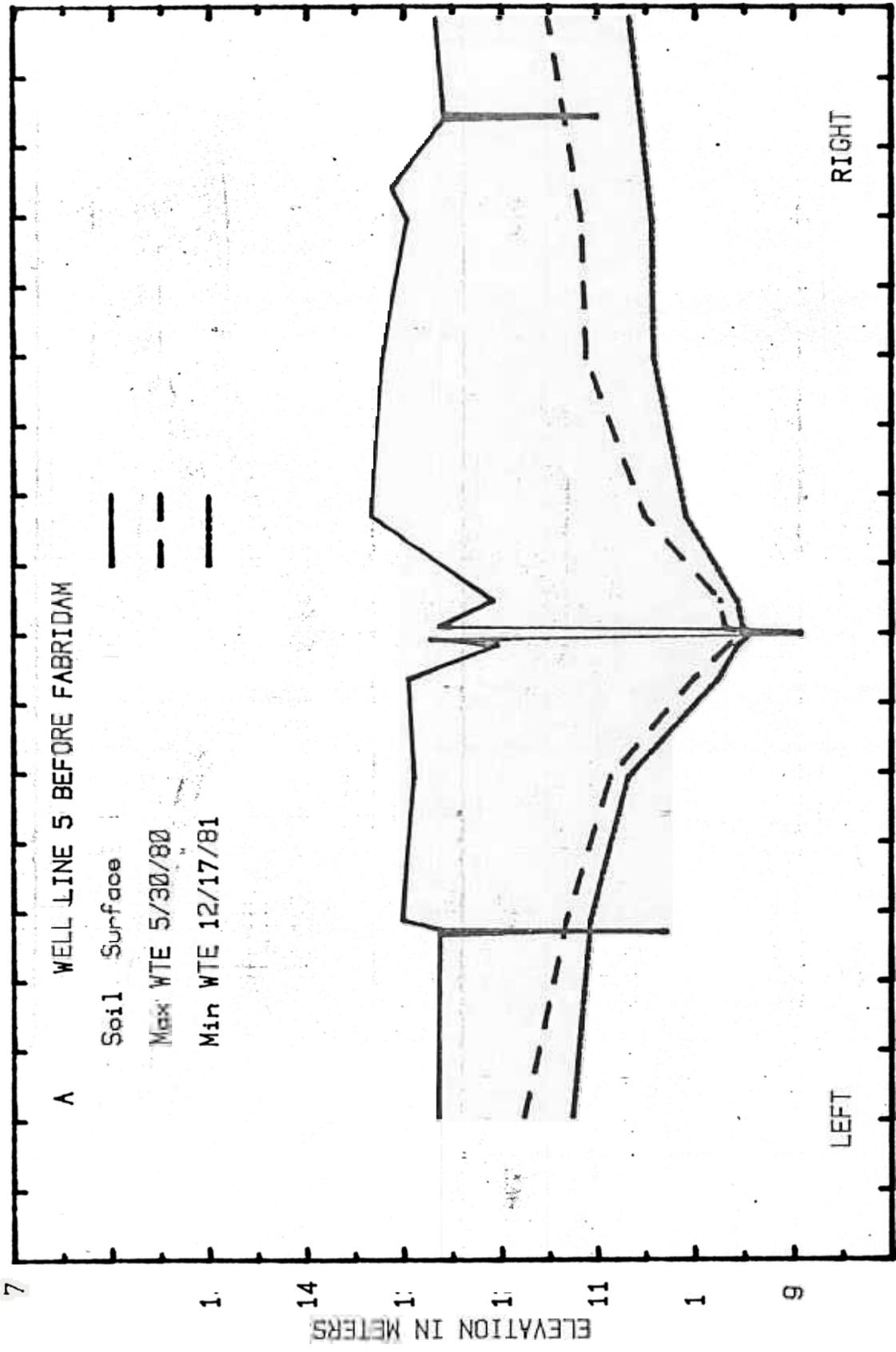


Fig 3 The Fabr dam n Mitchell Cr ek
looking up str.

a better picture is being prepared



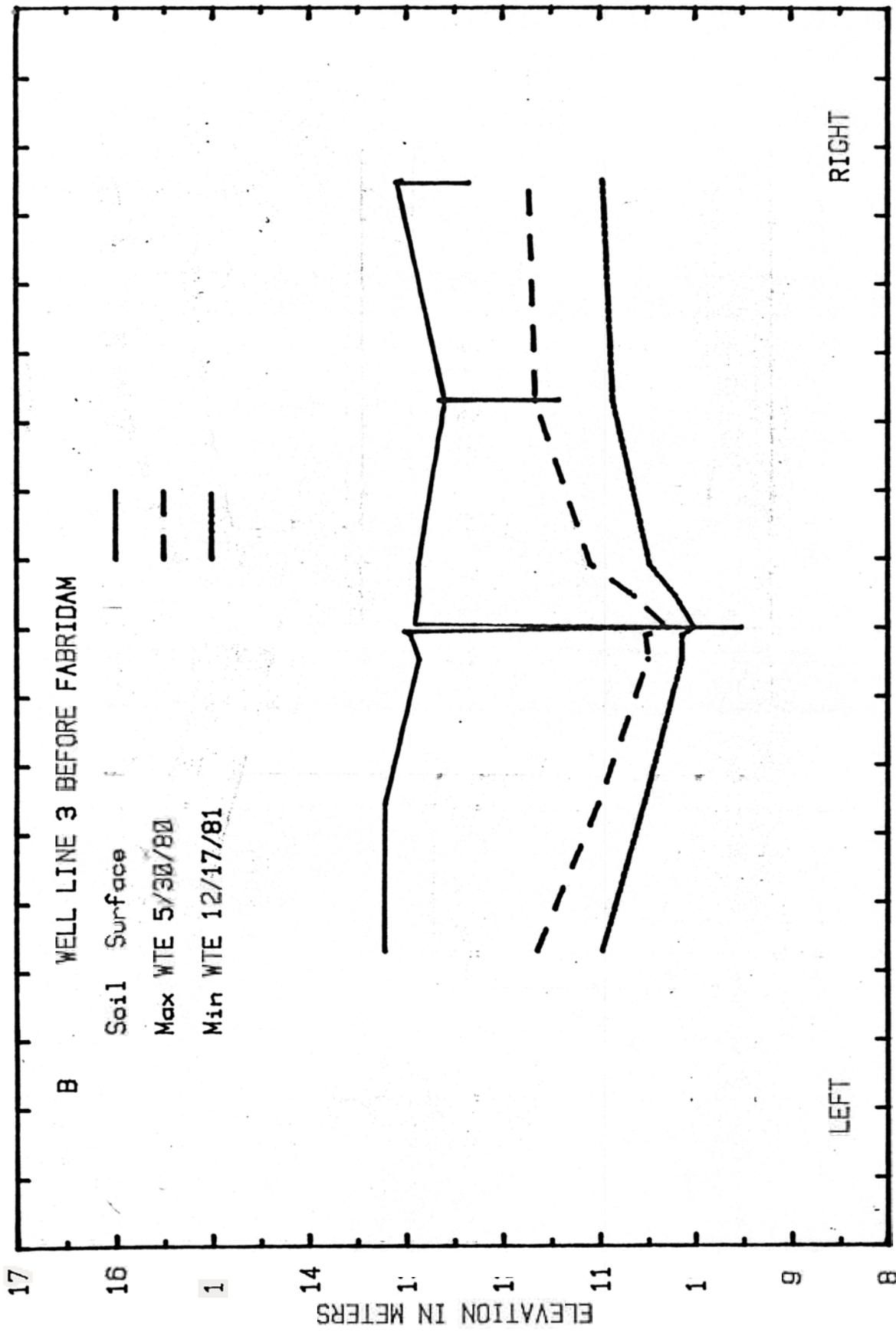
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STANCE FROM MTCHELL CREEK (m)

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in elevation

fig 4a

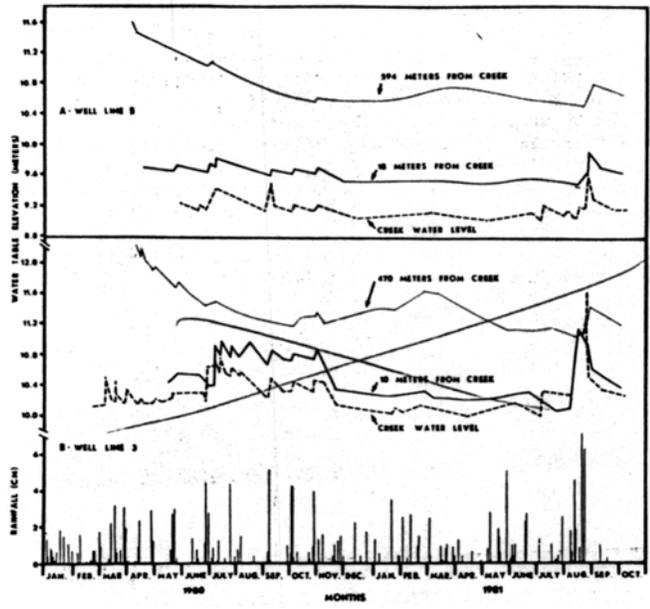


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Fig. 5. Relation of stream water elevation fluctuation to water table fluctuation near Mitchell Creek and at a distance away from Mitchell Creek at Well Line #5(A), and Well Line #3(B).

This figure will be changed to include the full year data for 1981, but will only include line 3

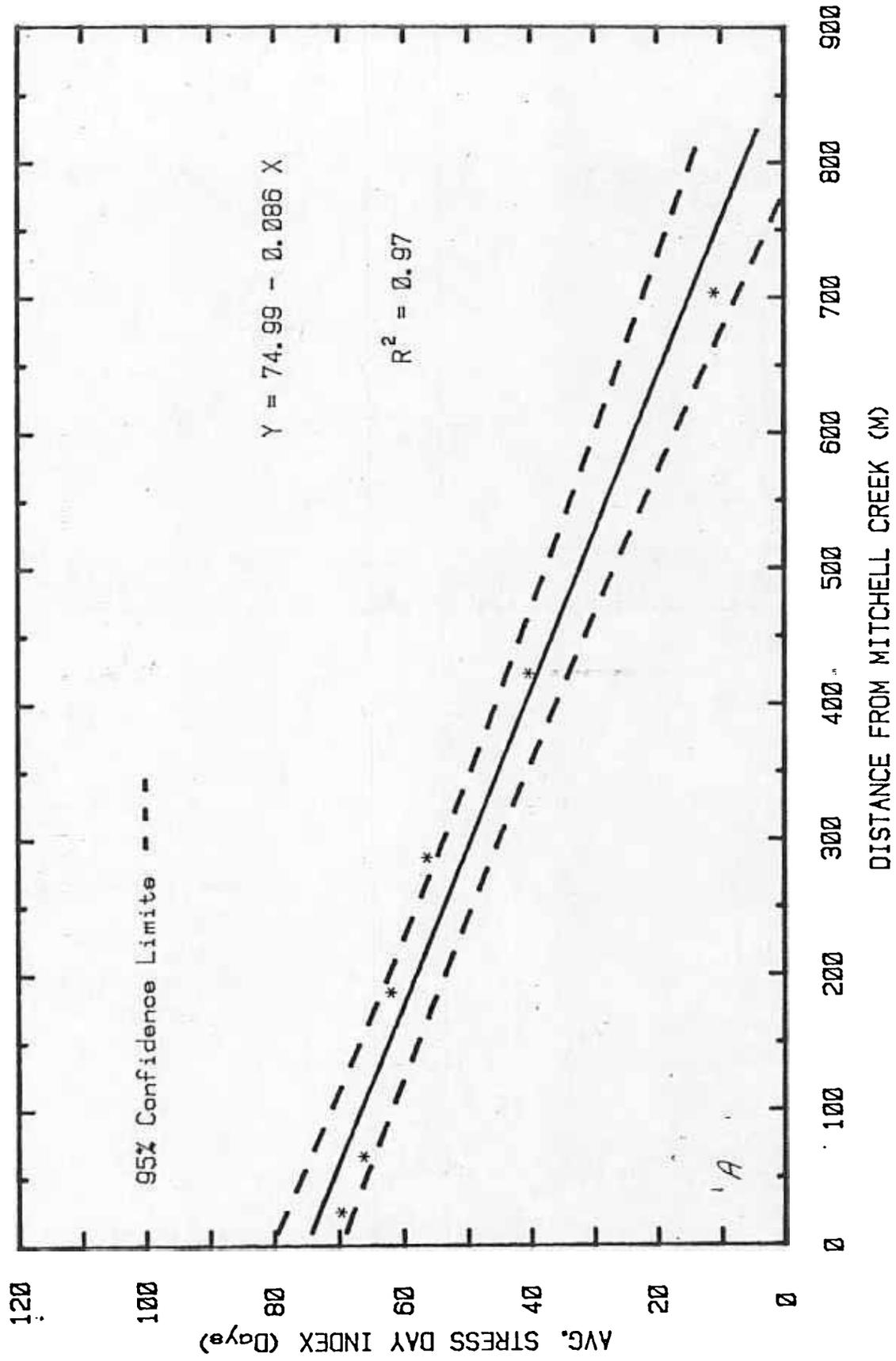


Fig. 6a. Relationship between average stress day index (SDI) and distance from Mitchell Creek for crop years 1980 and 1981.

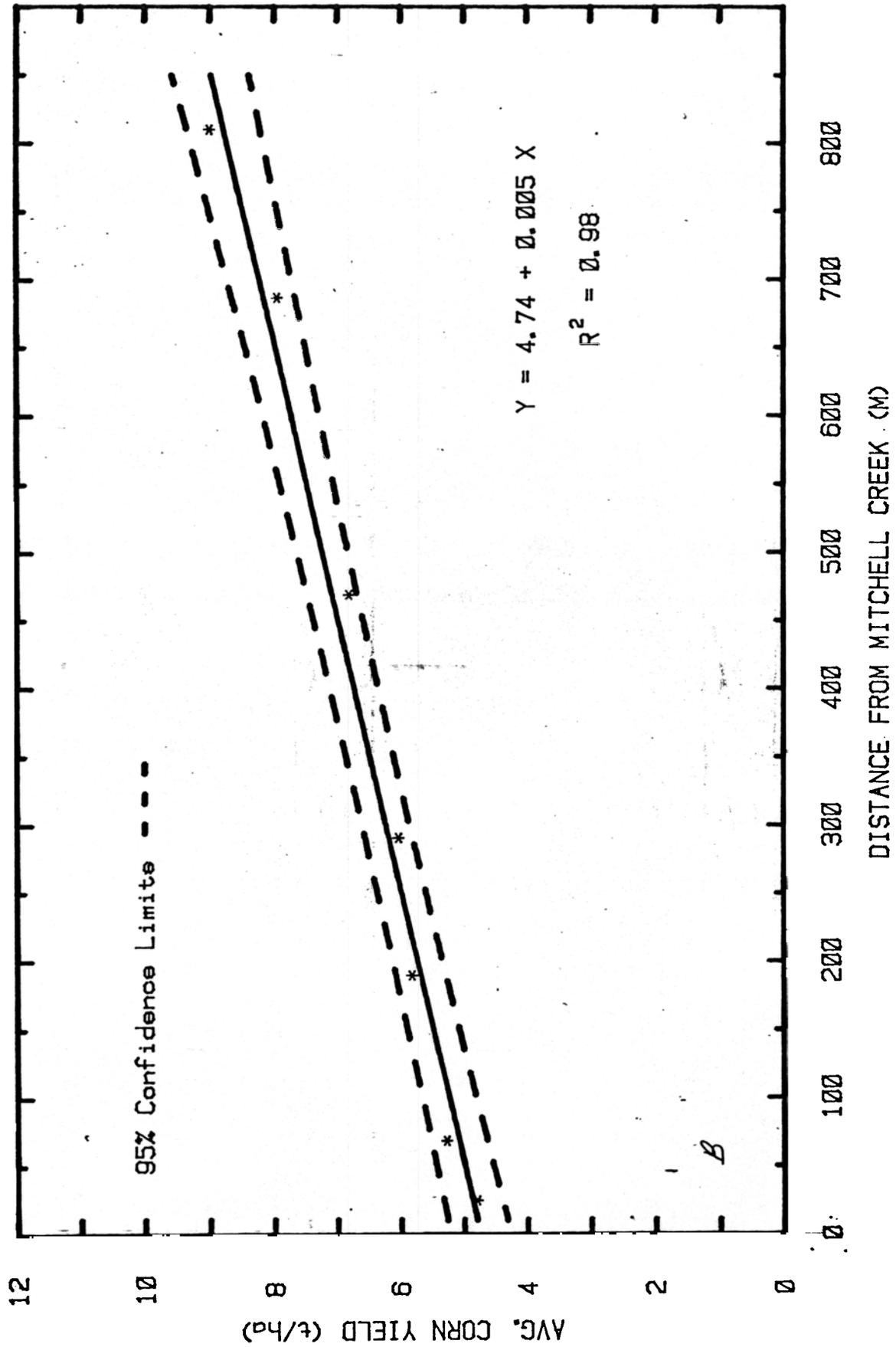


Fig. 6b. Relationship between average corn yield and distance from Mitchell Creek for crop years 1980 and 1981.

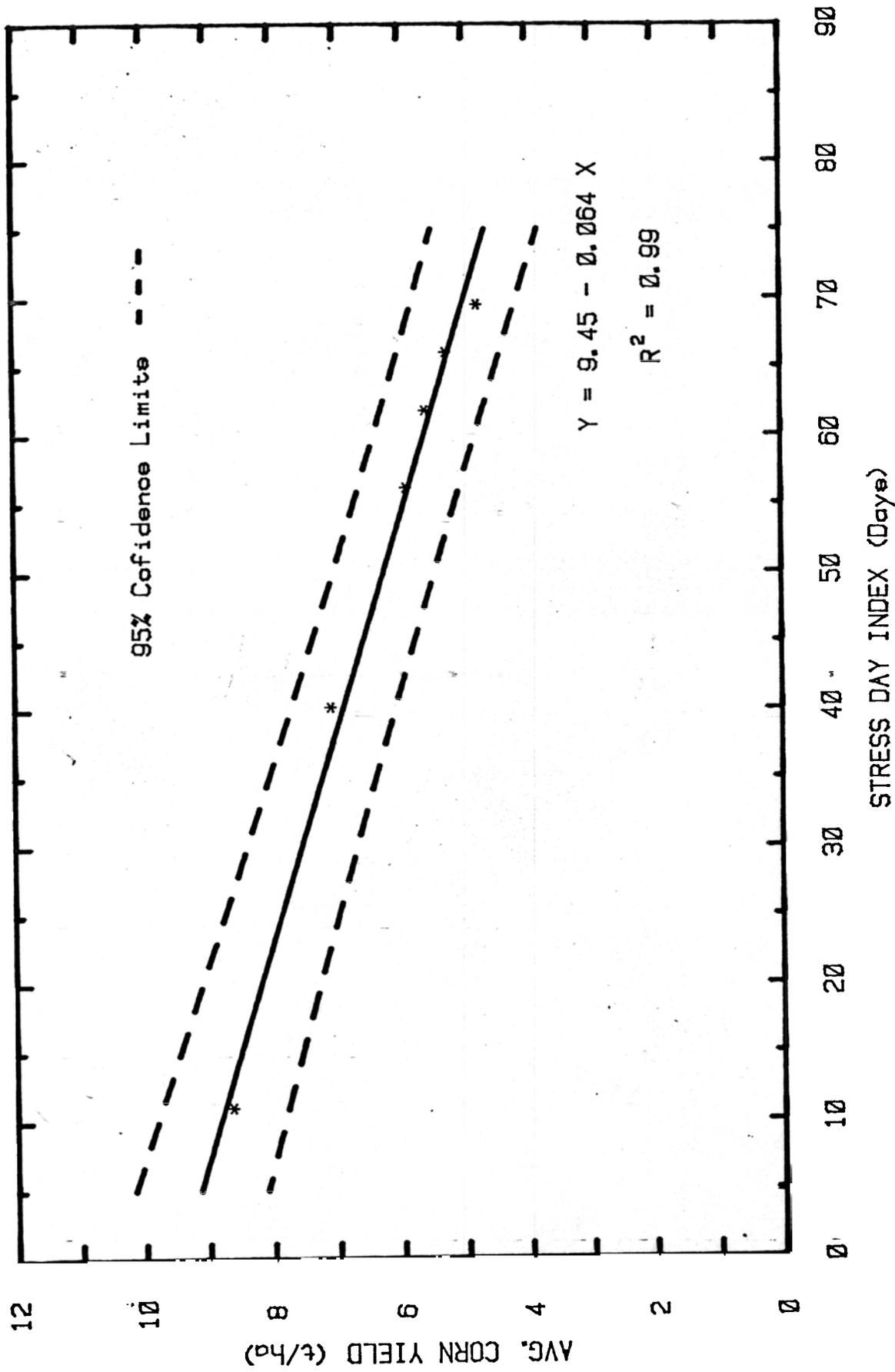


Fig. 7. Relationship of corn yield to stress day index for the 1980-81 growing seasons in sandy soils in the Mitchell Creek Watershed. The confidence limits are based on the full 17 data points, not the average 6 points shown.

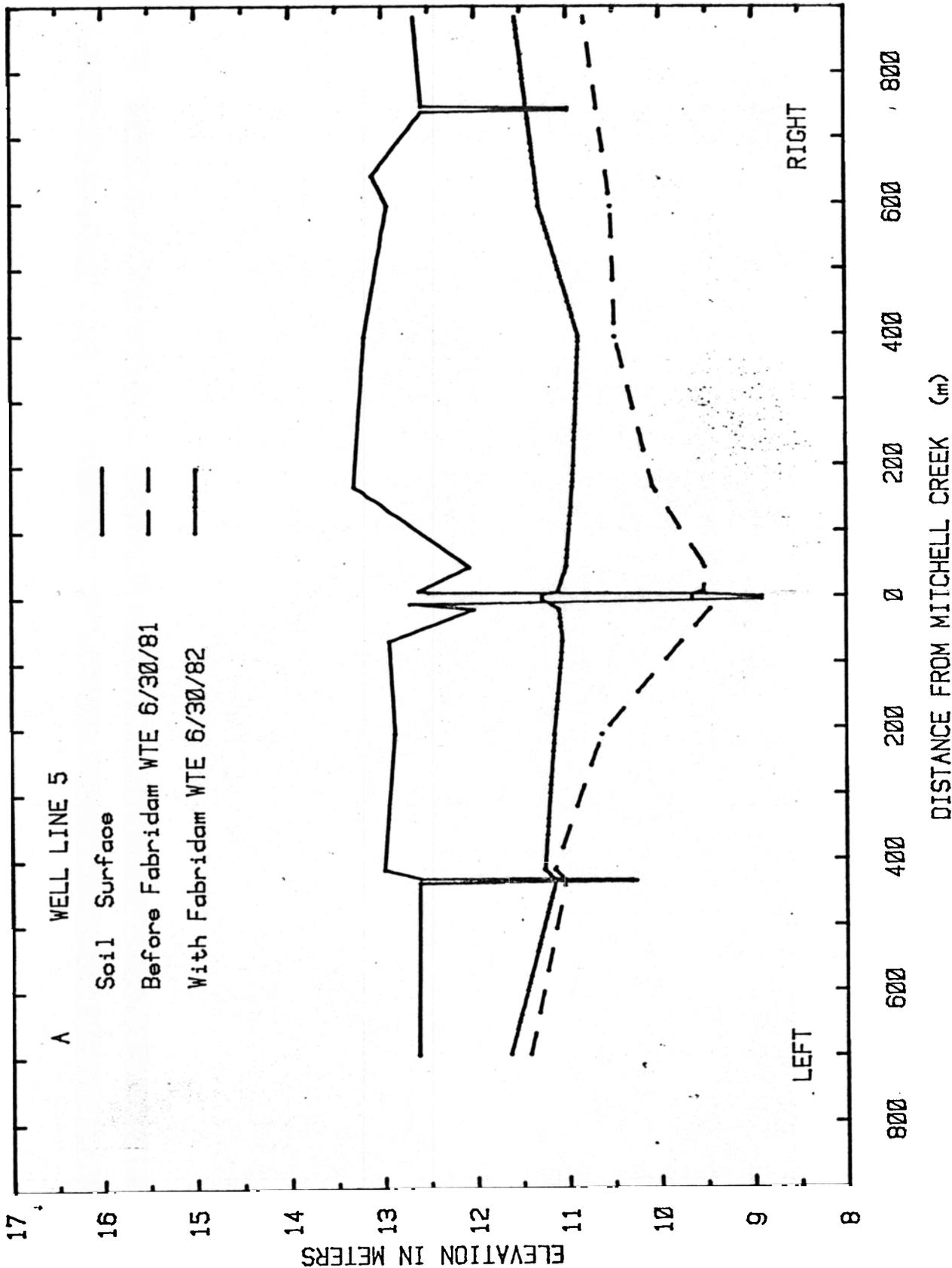


Fig. 18a. Water table above the Fabridam in relation to distance from Mitchell Creek for the high water use period for corn before the Fabridam, June 30, 1981, and after the Fabridam was installed to control the stream water level on June 30, 1982.

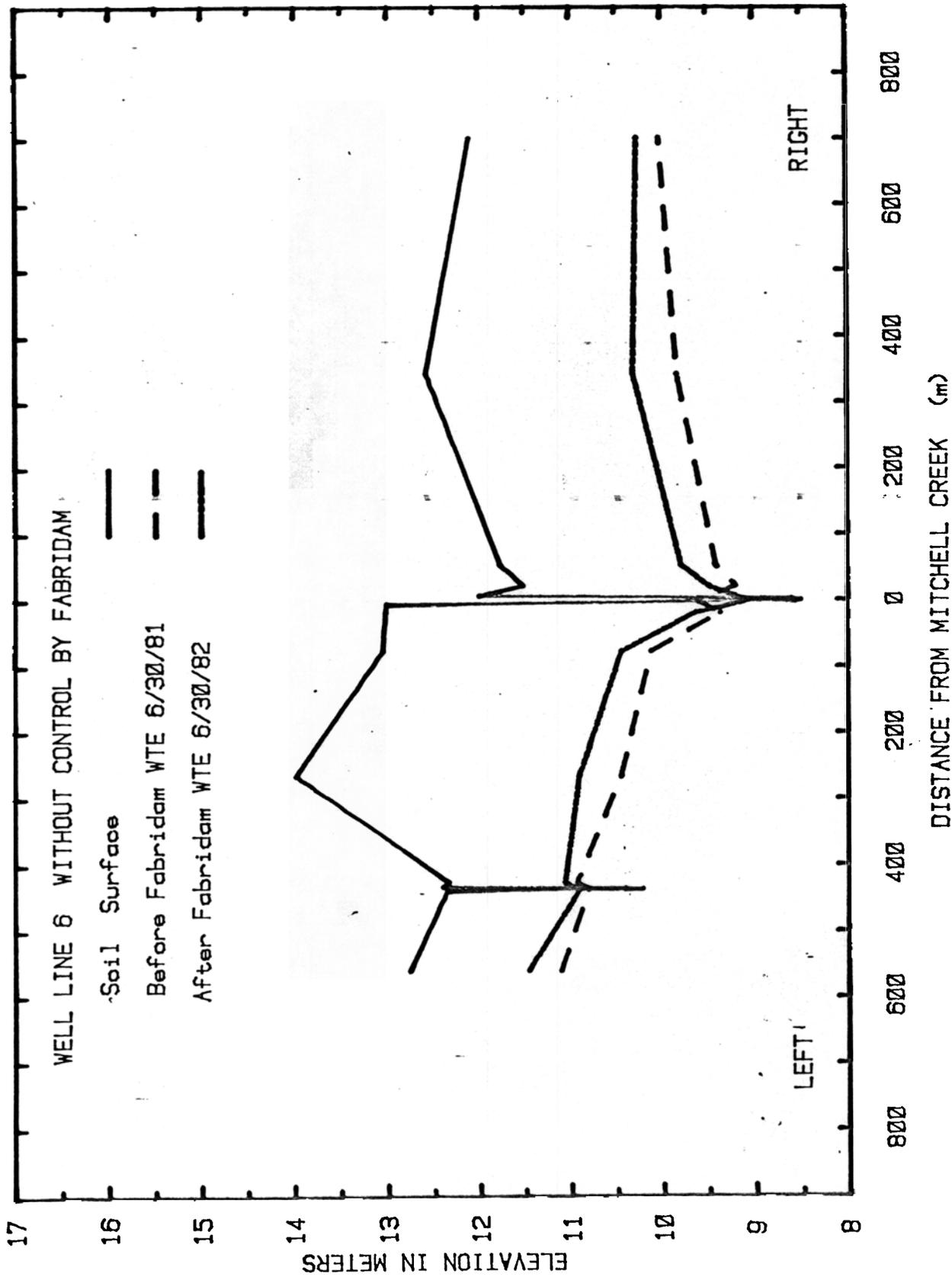
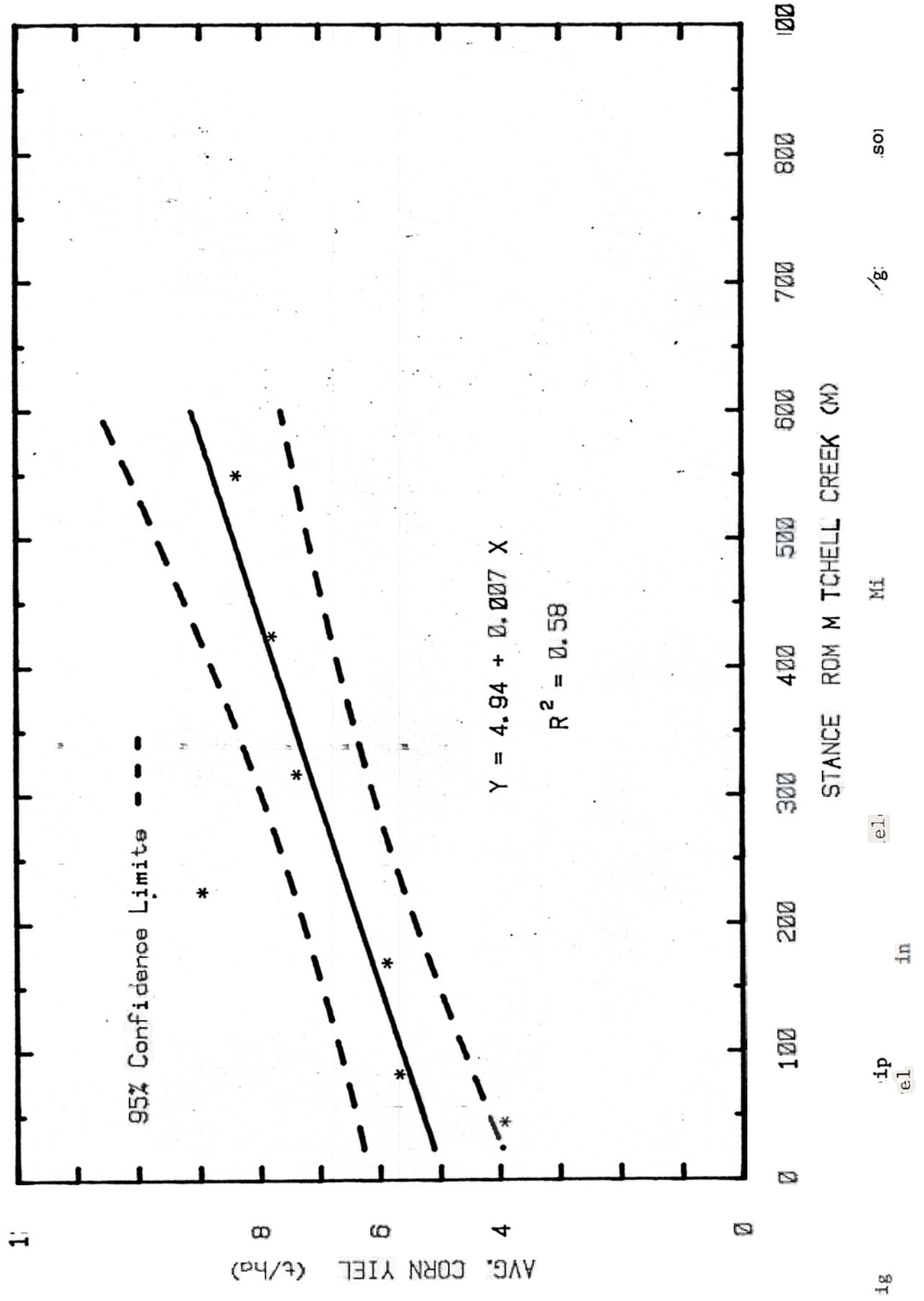


Fig. 8b. Water table below the Fabridam in relation to distance from Mitchell Creek for the high water use period for corn, June 30, 1981 and June 30, 1982.



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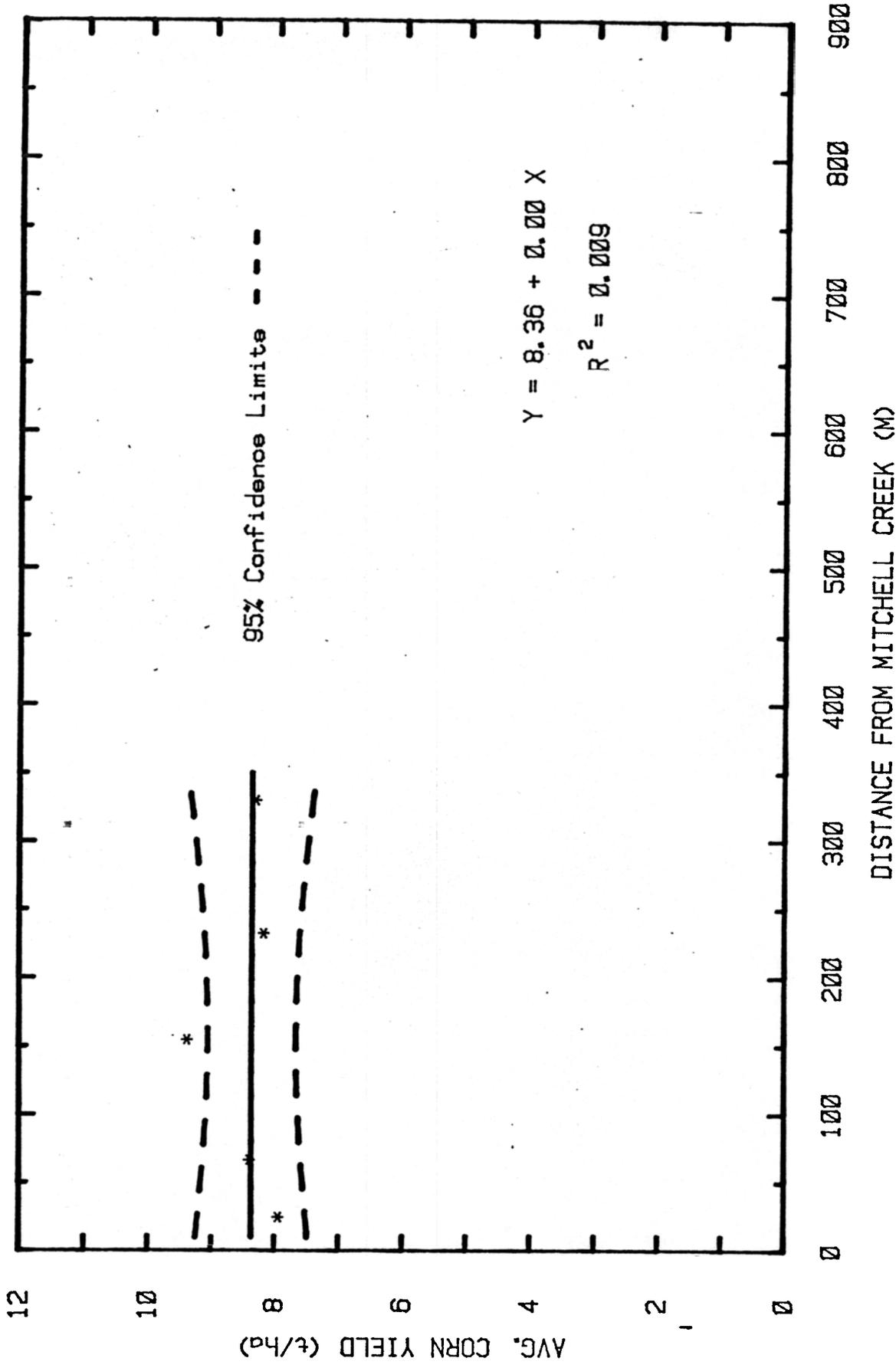
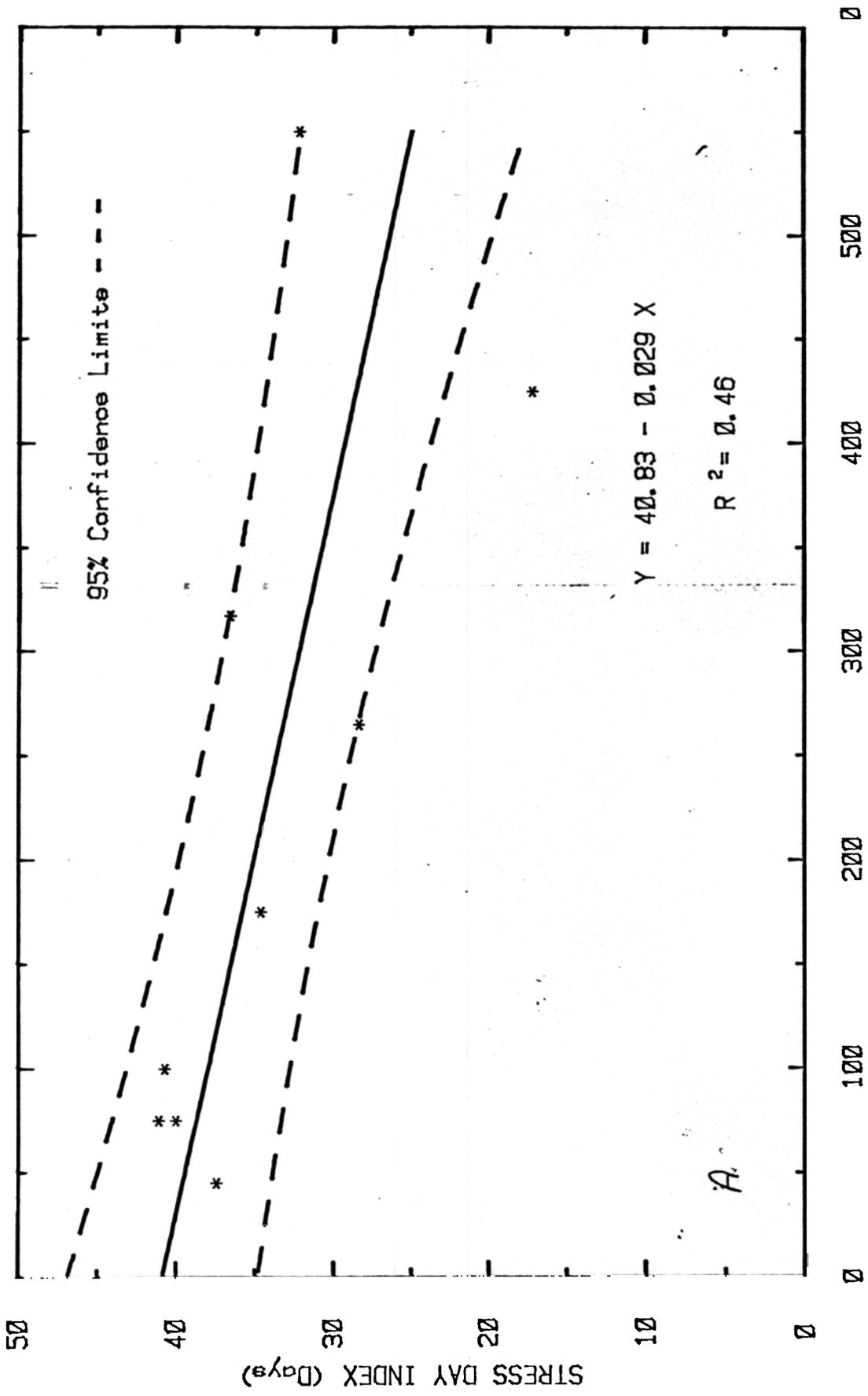


Fig. 9b. Relationship of average corn yield to distance from Mitchell Creek for the 1982 growing season, with water level control in the stream by the Fabridam.



DISTANCE FROM MITCHELL CREEK (M)

Fig. 10a. Relationship between average stress day index and distance from Mitchell Creek, with no water level control in the stream.

1982 WATER LEVEL CONTROL BY FABRIDAM

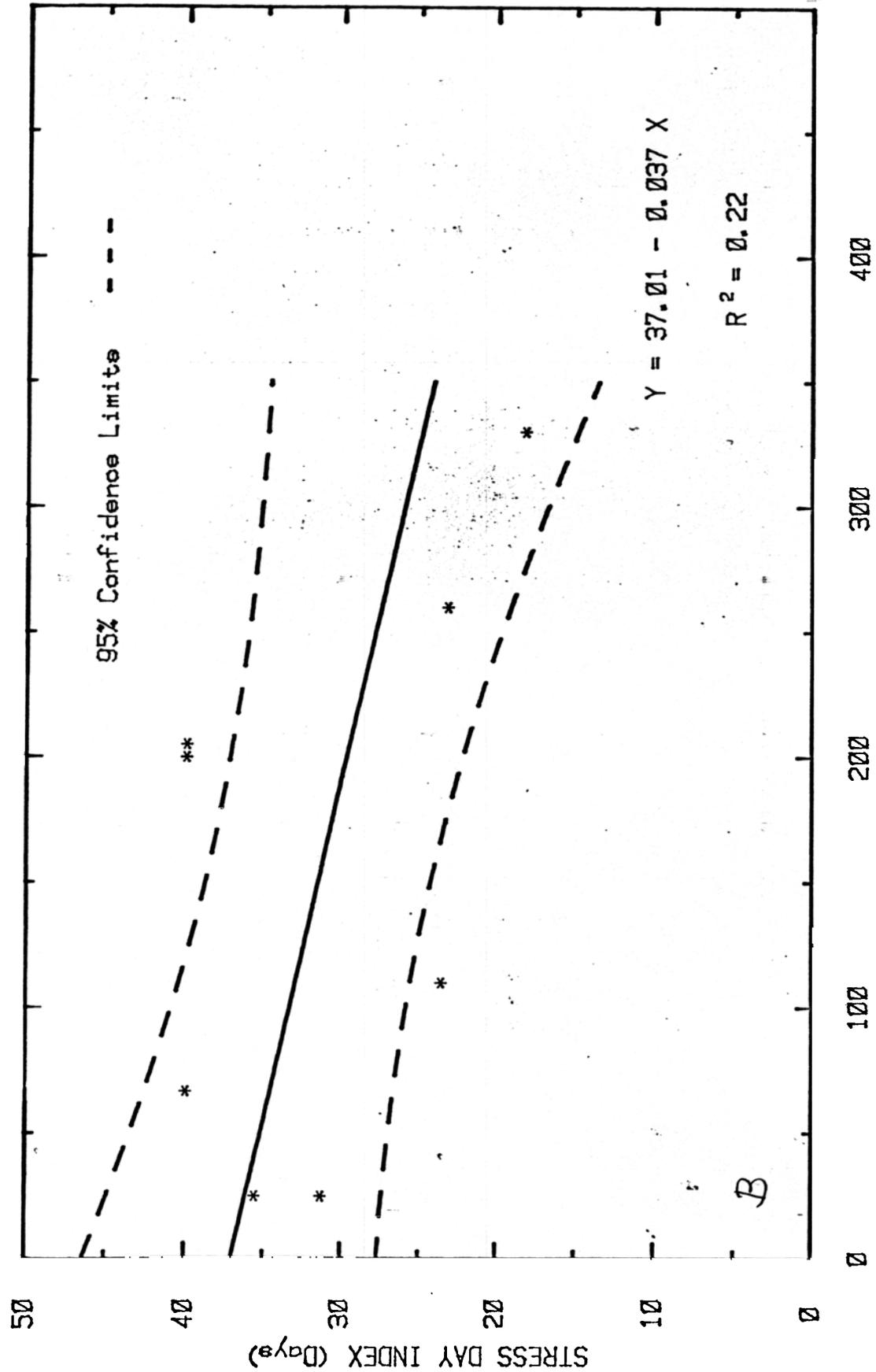
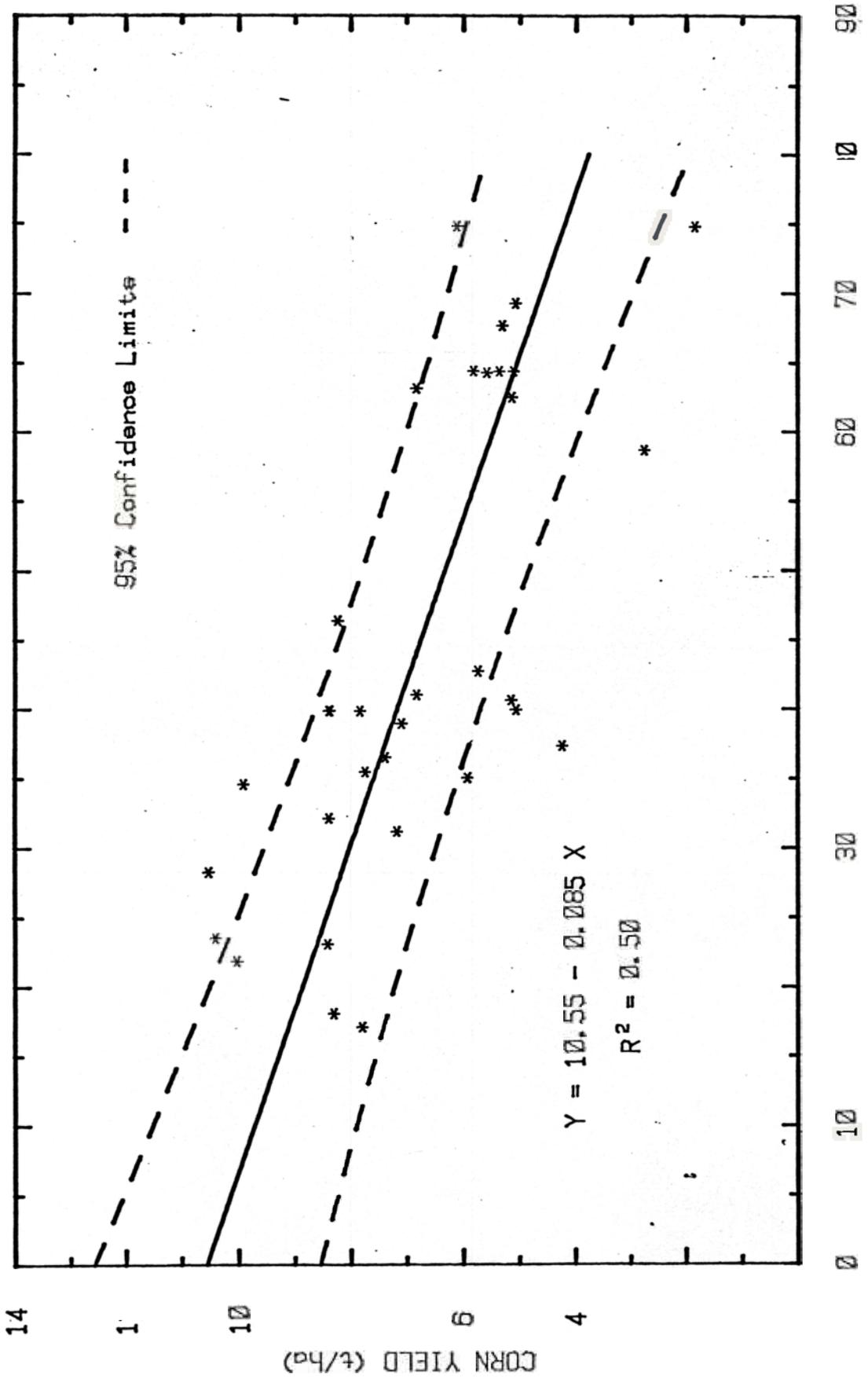


Fig. 10b. Relationship between average stress day index and distance from Mitchell Creek, with water level control in the stream by the Fabridam.



TRESS AY N (Days)